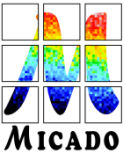


The MICADO derotator and its test stand at MPIA

S. Barboza, J.-U. Pott, F. Müller, R.-R. Rohloff, N. Muench,
R. Hofferbert, L. Mohr, F. Briegel, J. F. Wagner,
precision mechanical workshop MPIA

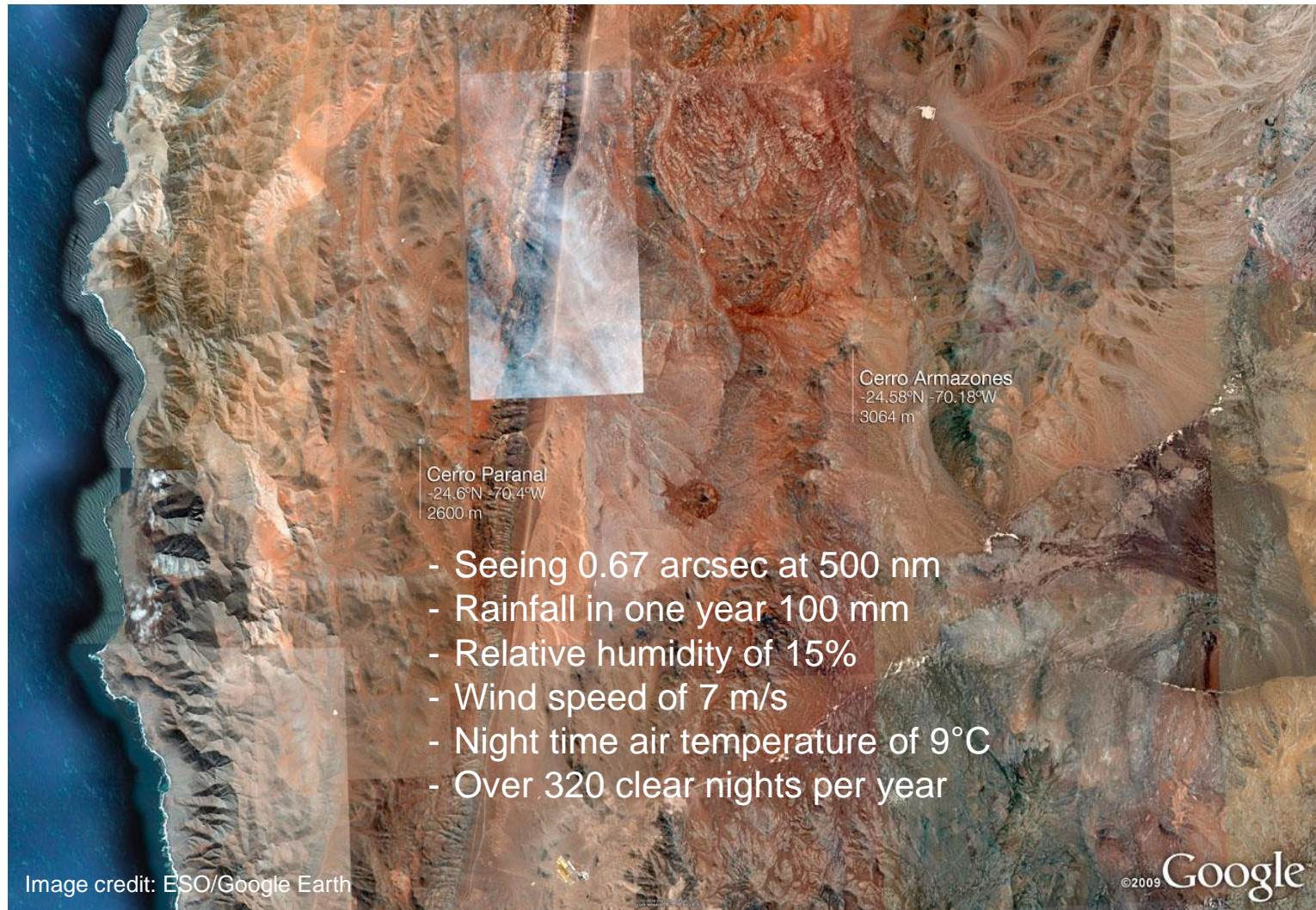
Astro Tech Talk
MPIA, 28 October 2016

Outline



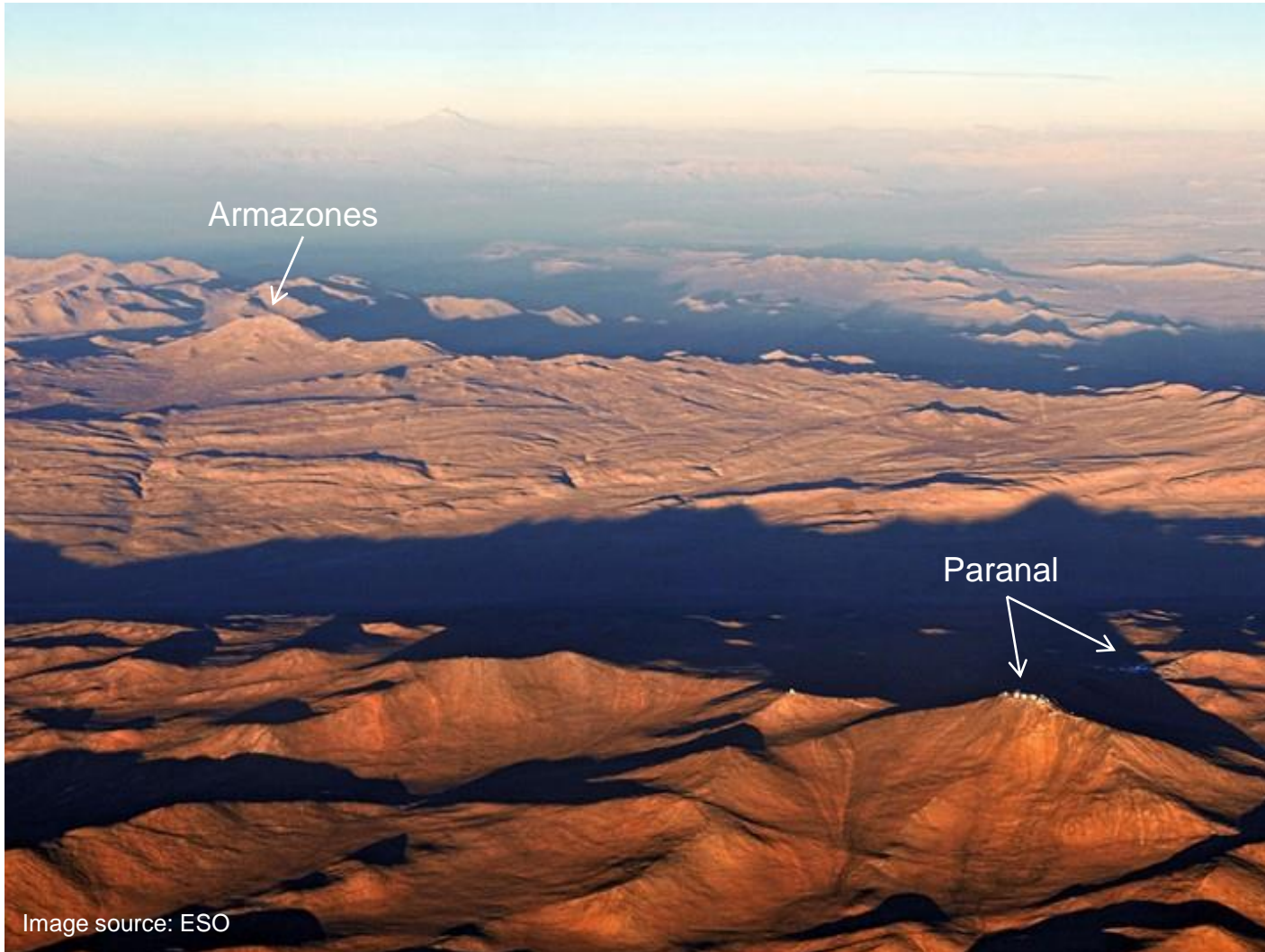
- European Extremely Large Telescope (E-ELT)
- MICADO
- Why a Derotator is needed
- The Derotator concept
- Test stand and the integration process
- Integration status and missing components
- Goals of the experiment (kick-off)
- Planning for the test campaign
- Implementation schedule of the test campaign
- Tests already performed

- Location



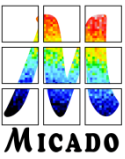
E-ELT

- Location

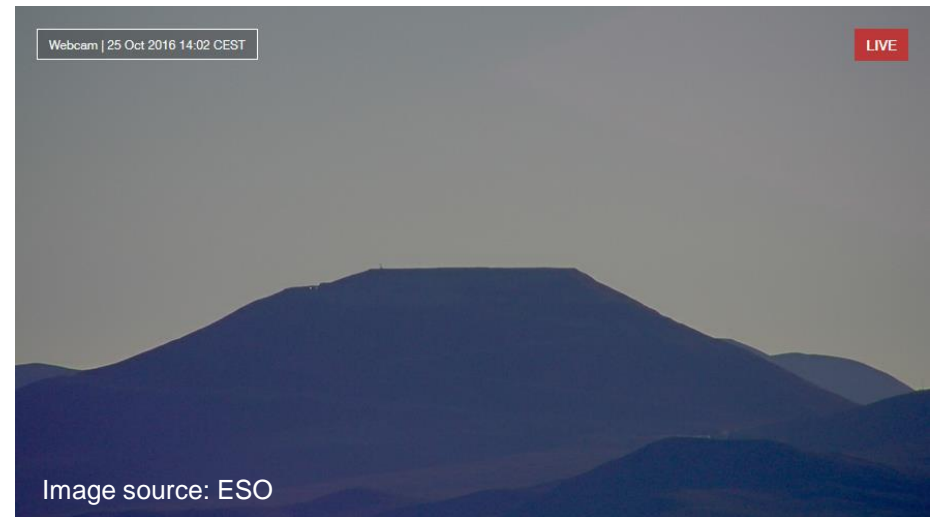


Atacama Desert, Chile

E-ELT



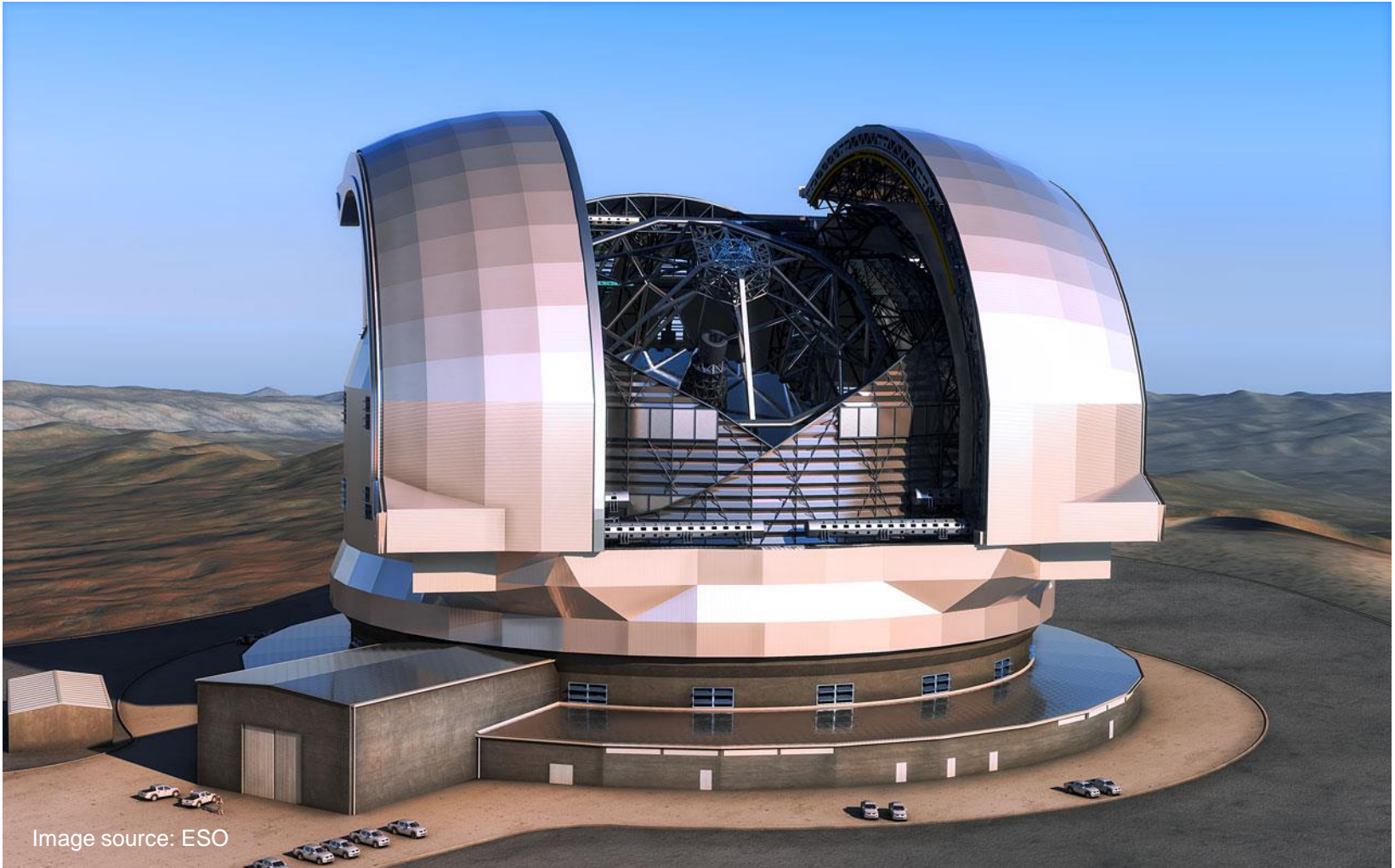
- Location



Atacama Desert, Chile

E-ELT

- Green light for E-ELT construction “Phase 1”
(see organization release eso1440 - The Messenger 158, December 2014)



ELT rendering Atacama Desert, Chile

E-ELT

- In May 2016 ESO signed the contract for E-ELT Dome and Telescope Structure (see organization release eso1617)



Atacama Desert, Chile

- Instruments and adaptive optics modules

Name	Instrument Type	Wavelength Range	Field of View
CODEX	High Resolution, High Stability Visual Spectrograph	0.37 – 0.71 μ m	0.82"
EAGLE	AO-assisted Multi-integral Field NIR Spectrometer	0.8 – 2.45 μ m	IFU: 1.65" x 1.65"
EPICS	Planet Imager, Spectrograph and Imaging Polarimeter with Extreme Adaptive Optics	0.6 – 1.65 μ m	IFU: 0.8" x 0.8"
HARMONI	Single Field Integral-field Spectrograph	0.47 – 2.45 μ m	10" x 5" with the coarsest pixel scale
METIS	Mid-infrared Imager and Spectrograph with AO	2.9 – 14 μ m	17.6" x 17.6" (imager)
MICADO	Imager and Slit Spectrograph	0.8 – 2.5 μ m	up to 53"
OPTIMOS-DIORAMAS	Wide-Field Imager & Low-Medium Resolution Slit Spectrograph	0.37 – 1.6 μ m	6.78' x 6.78'
OPTIMOS-EVE	Optical-NIR Fibre-based MOS	0.37 – 1.7 μ m	Large field IFU: 7.8" x 13.5"
SIMPLE	Cross-dispersed Echelle Spectrograph, Long-slit Option	0.8 – 2.5 μ m	up to ~4" patrol field for slit viewer
ATLAS	Laser Tomography AO Module	0.35 – 13.5 μ m	60"
MAORY	Multi Conjugate AO Module	0.8 – 2.4 μ m	2'

MICADO Kick-Off

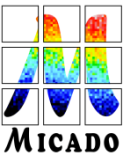


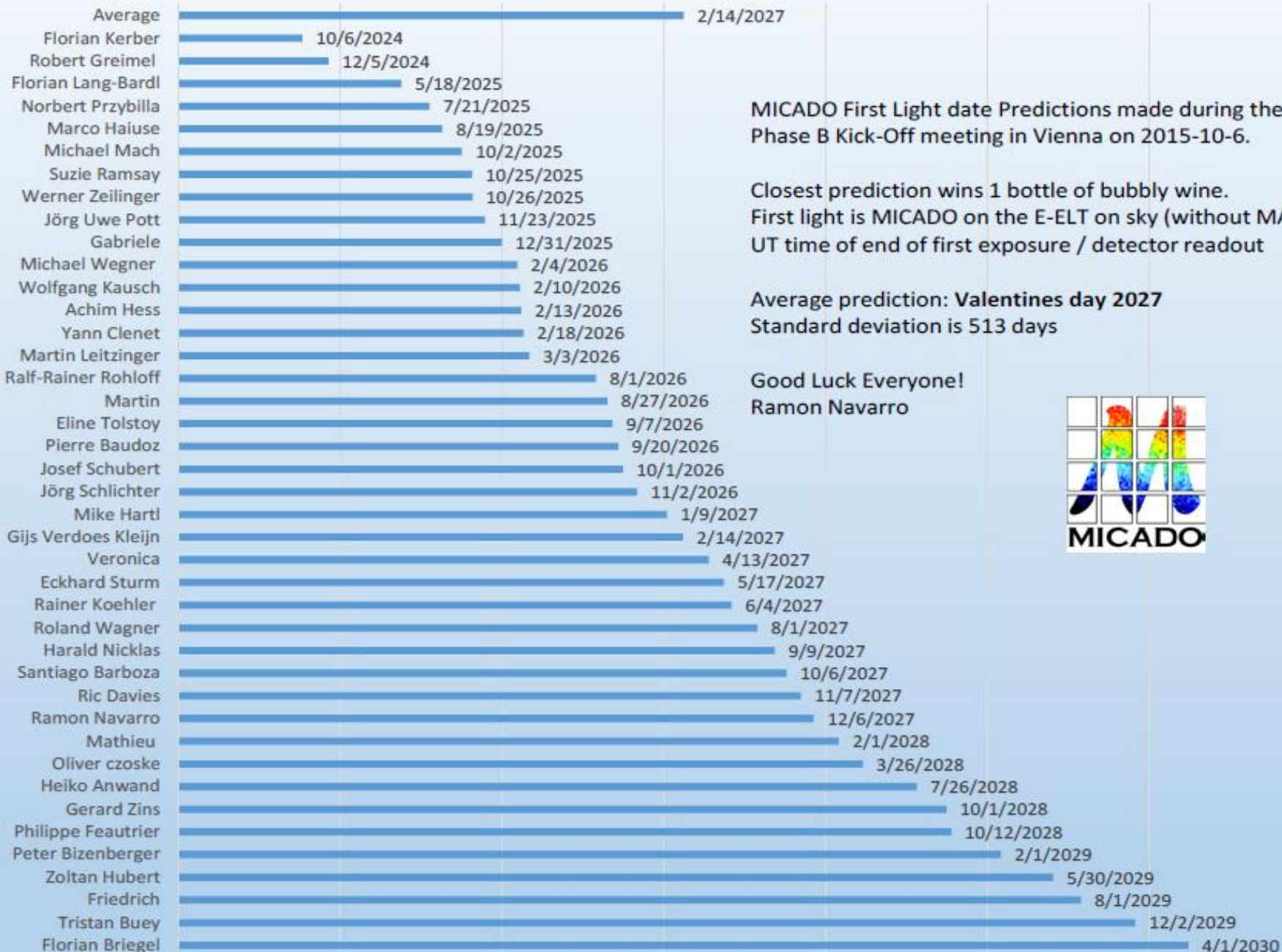
Image source: MPE/MICADO Consortium

Image of the consortium taken at the MICADO kick-off meeting in Vienna, 7 October 2015

- Preliminary Design Review, October 2018
- Final Design Review, 2020
- Preliminary Acceptance Europe, 2023
- First Light, 2024

MICADO official First Light date prediction contest

1/1/2024 1/1/2025 1/1/2026 1/1/2027 1/1/2028 1/1/2029 1/1/2030 1/1/2031



MICADO First Light date Predictions made during the Phase B Kick-Off meeting in Vienna on 2015-10-6.

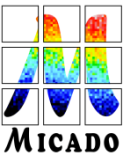
Closest prediction wins 1 bottle of bubbly wine.
First light is MICADO on the E-ELT on sky (without MAORY).
UT time of end of first exposure / detector readout

Average prediction: **Valentines day 2027**
Standard deviation is 513 days

Good Luck Everyone!
Ramon Navarro



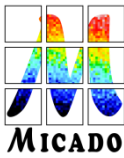
MICADO



- Located in the straight focal station on the Nasmyth platform



MICADO



- The Multi-AO Imaging CAmera for Deep Observations

- Key Capabilities

- Sensitivity and resolution
- Precision astrometry
- Spectroscopy
- Simple and robust

- The instrument design has been optimized for MCAO (MAORY)

- Large 53 arcsec field of view at the diffraction limit of the E-ELT

- The early operational phase will use SCAO (if MAORY is not ready)

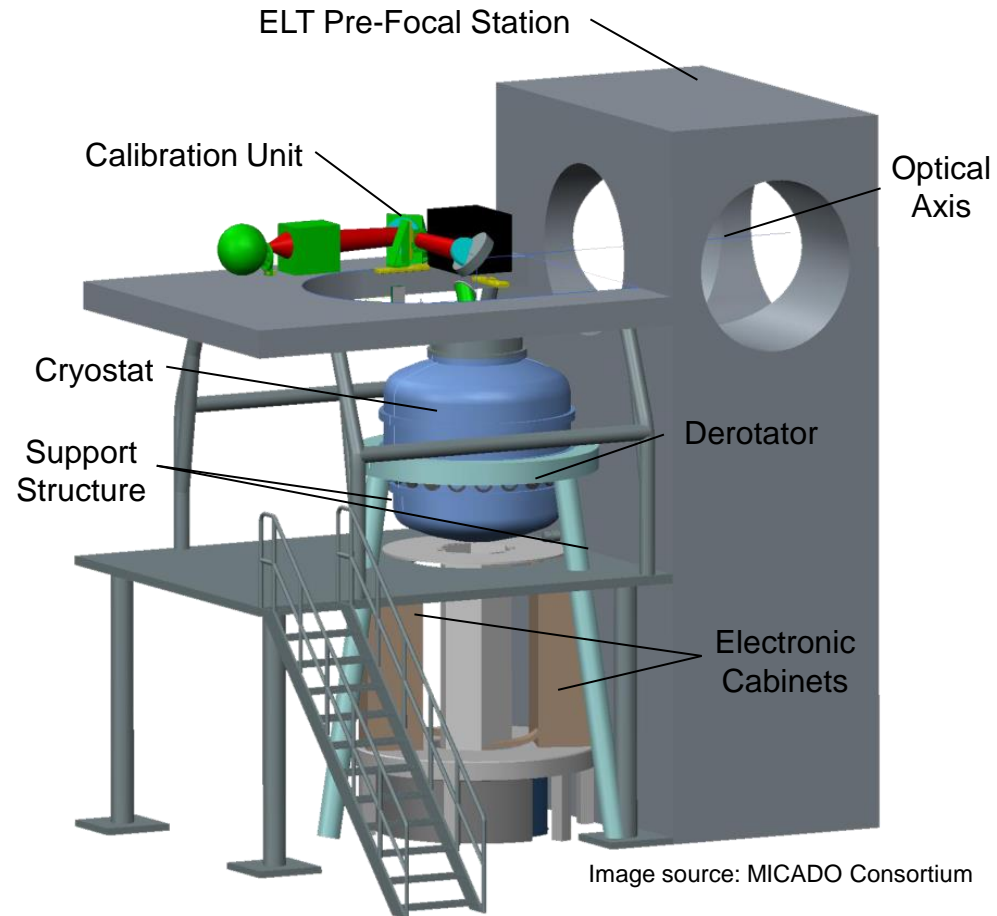


Image source: MICADO Consortium

MICADO- MAORY

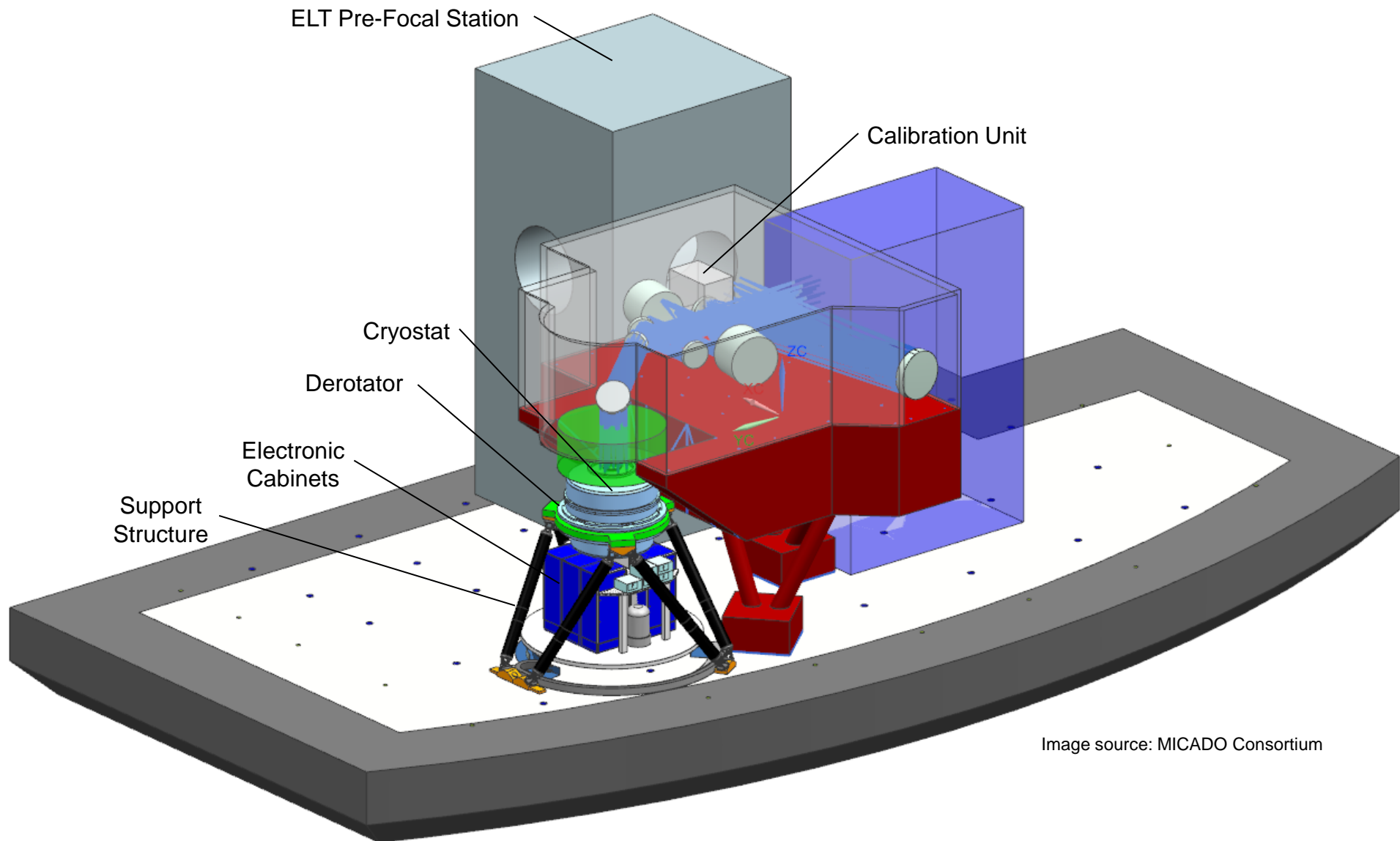
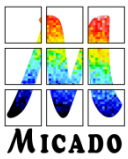


Image source: MICADO Consortium

Why a Derotator is needed?

- Field rotation on telescopes with Alt-Azimuth mounts

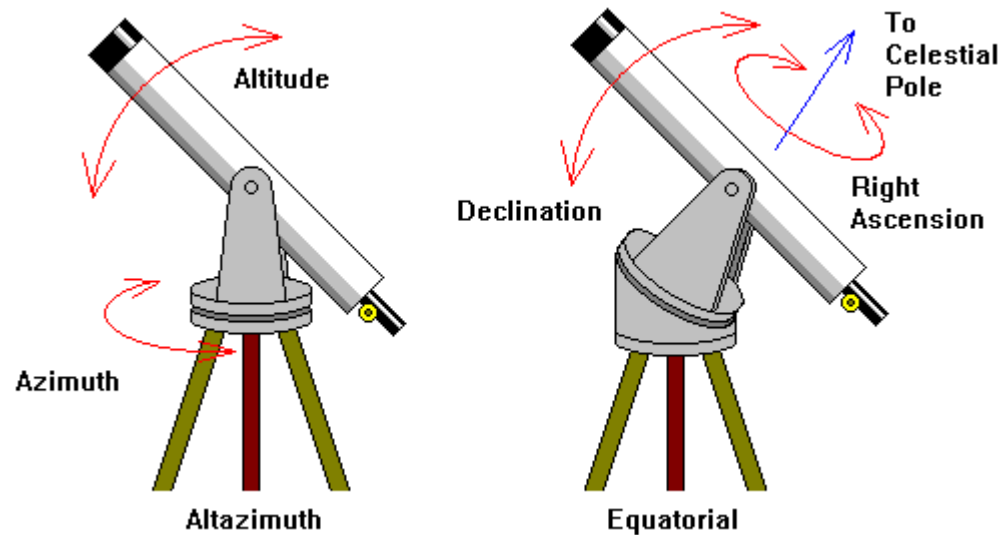


Image source: www.oasi.org.uk



Images with short-exposure time

Why a Derotator is needed?

- Field rotation on telescopes with Alt-Azimuth mounts



Images with long-exposure time

Why a Derotator is needed?

- Field rotation on telescopes with Alt-Azimuth mounts



Images with long-exposure time

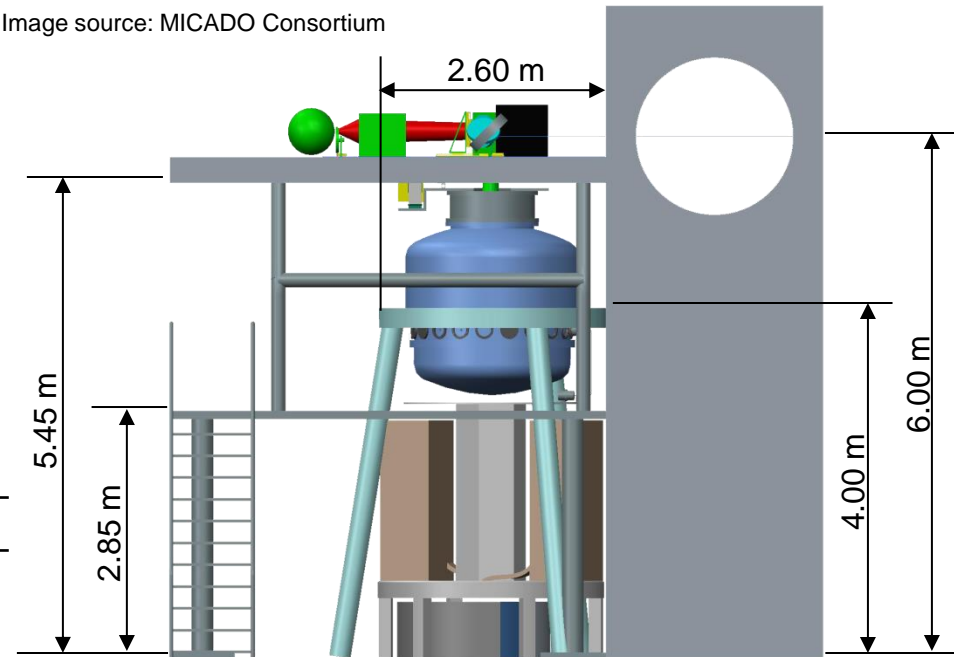
The Derotator

- Bearing, drivers, motors, encoders and mechanical interfaces
- High precision requirements
- How to achieve (if possible) 1 arcsec of rotational positioning accuracy ?

Parameter	Value
Inner diameter	> 2100 mm
Thickness	≤ 230 mm
Moving mass	≤ 4 ton
Axial runout	< 50 μm
Radial runout	< 100 μm
Wobble	< 10 arcsec
Operating temperature	-10°C to 20°C
Rotation speed	360° in ≤ 2 min
Relative angular positioning accuracy	<10 arcsec (rms)

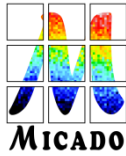
Derotator preliminary requirements

Image source: MICADO Consortium

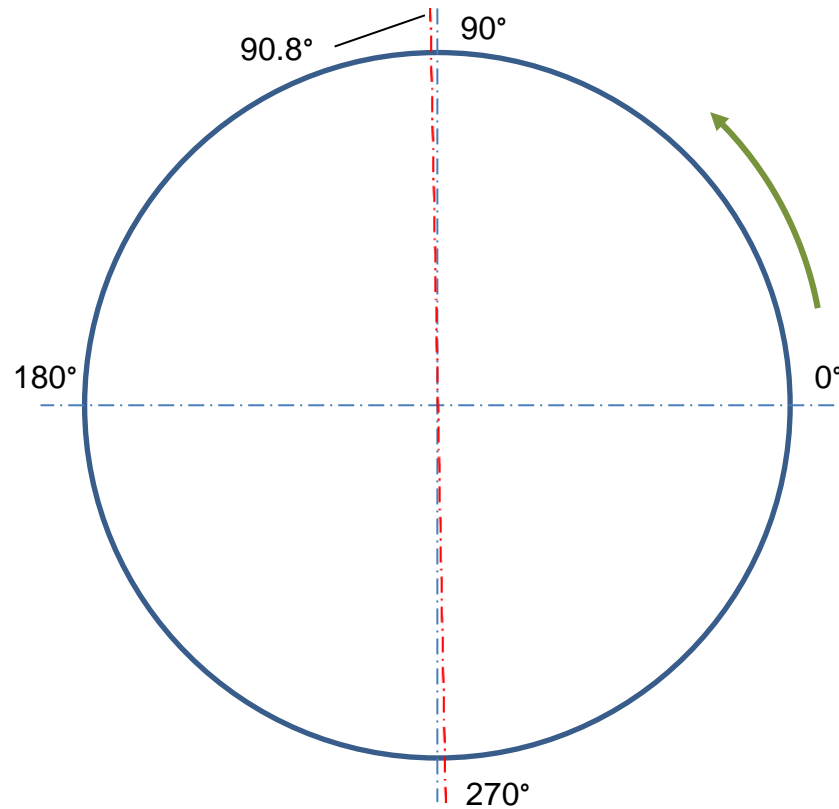


- Possible bearing technologies
 - Slewing bearings
 - Hydrostatic bearings
 - Air bearings
 - Magnetic bearings

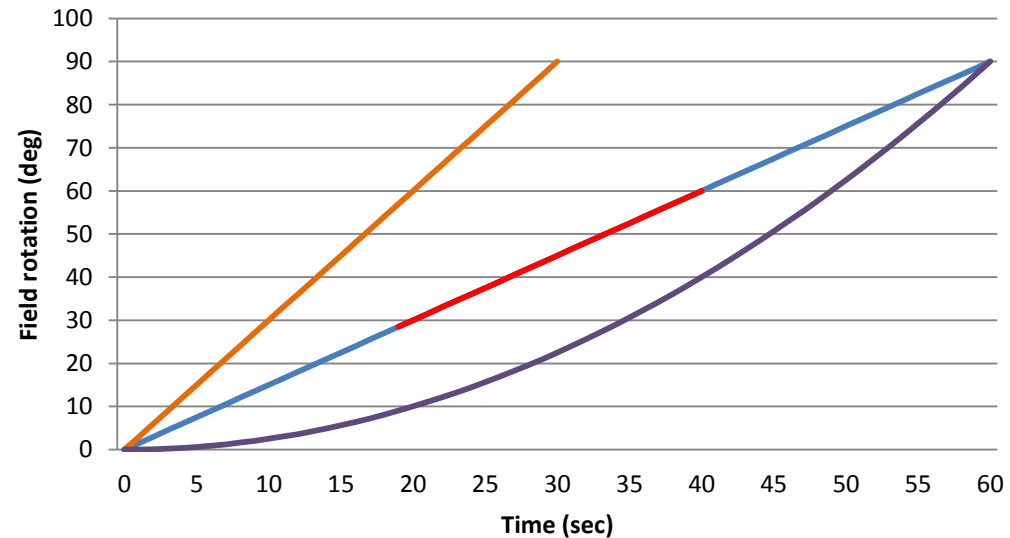
How accurate must be the Derotator?



- What does relative angular positioning accuracy mean?
- How much is 10 arcsec (rms)?



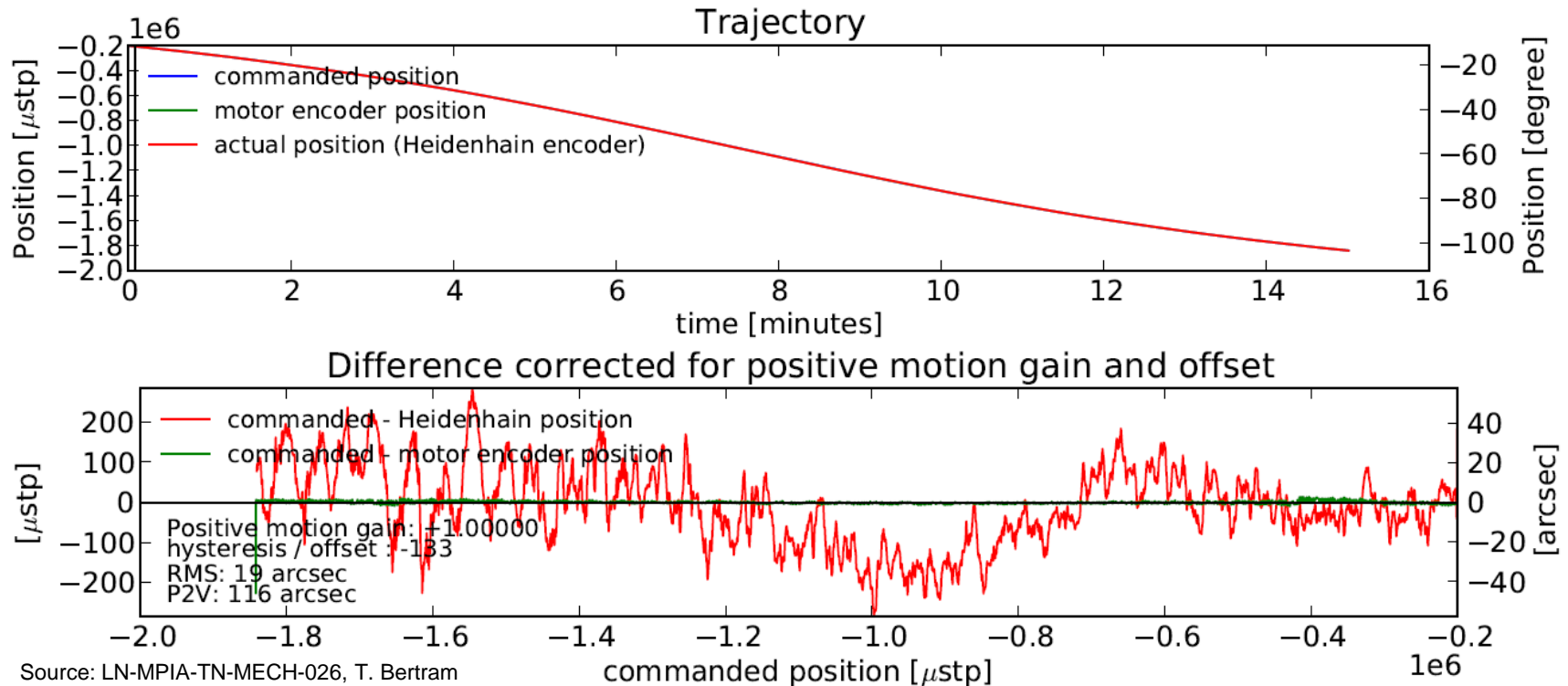
Derotator Trajectory



- Input = 90° → Output = 90.8° or 89.2° (measured position)
 - Absolute accuracy < 1° (Input – Output)
- 1 arcsec = 1°/3600 = 0.000287° → 10 arcsec = 0.00278°

LINC-NIRVANA GWS

- Bearing \varnothing 852 mm
- System working in open loop



Source: LN-MPIA-TN-MECH-026, T. Bertram

The Derotator Concept

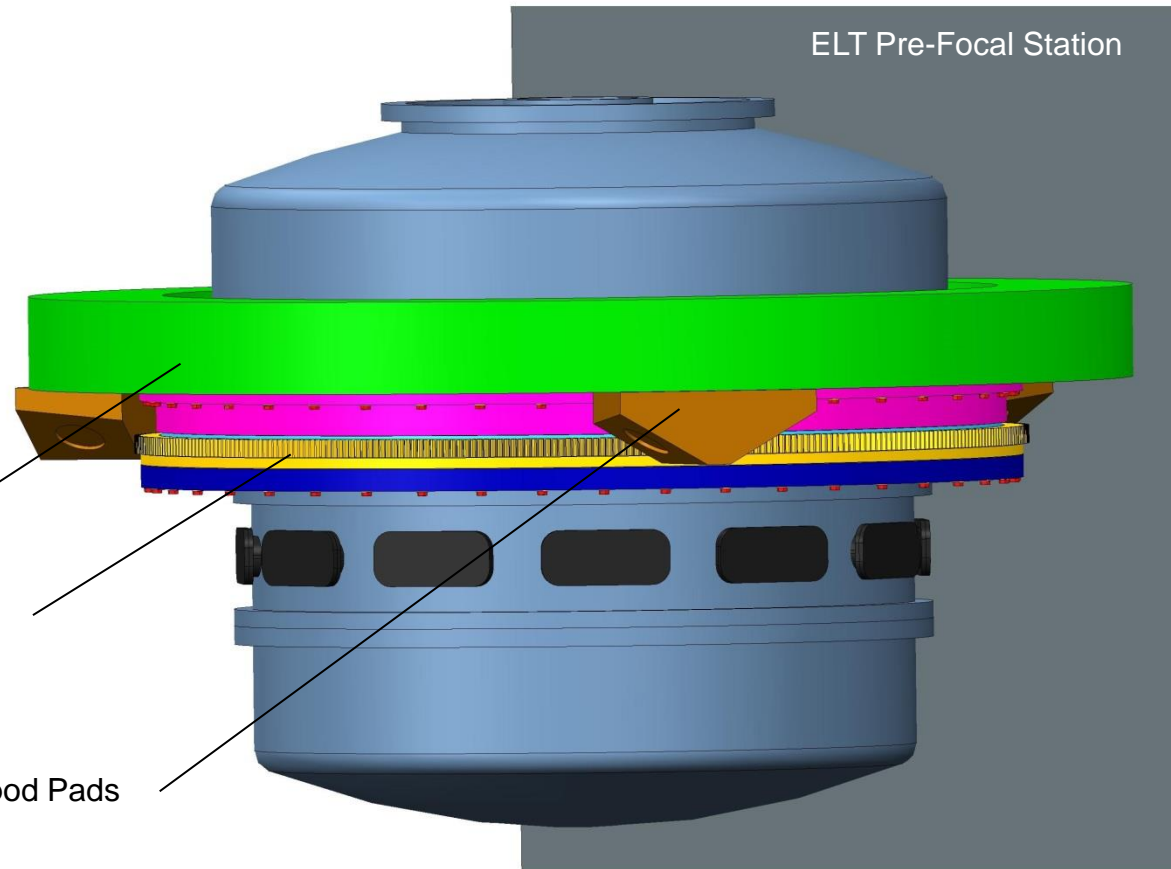
- Using Rhothe Erde Ball Bearing 83244820 (Gear Module 6)
 - Radial/Axial runout < 30 μm (requirement 100 μm / 50 μm)
- Based on a three points interface to the instrument support structure

Item	Mass (Kg)
Support Structure Interface	1446
Bearing support ring	311
Bearing	484
Drive unit	35
Drive unit	35
Encoder unit	16
Bolt and washers	34
Total	2361

Support Structure Interface

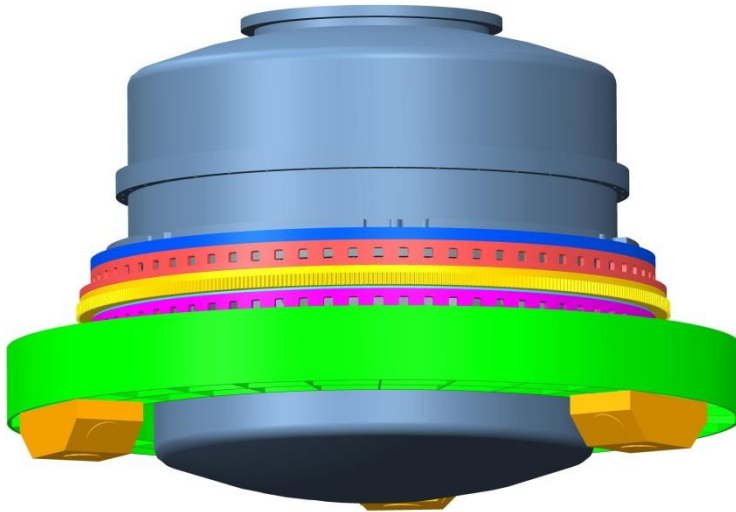
Bearing

Hexapod Pads

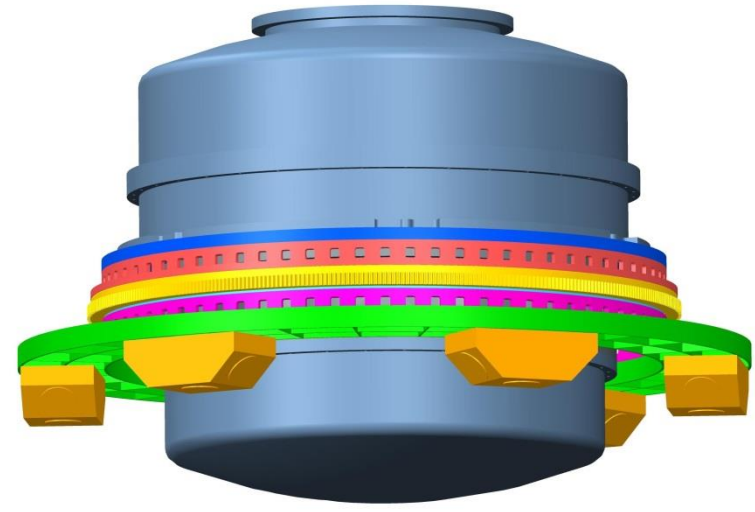


MICADO Derotator concept (support structure and motors not shown)

The Derotator Concept



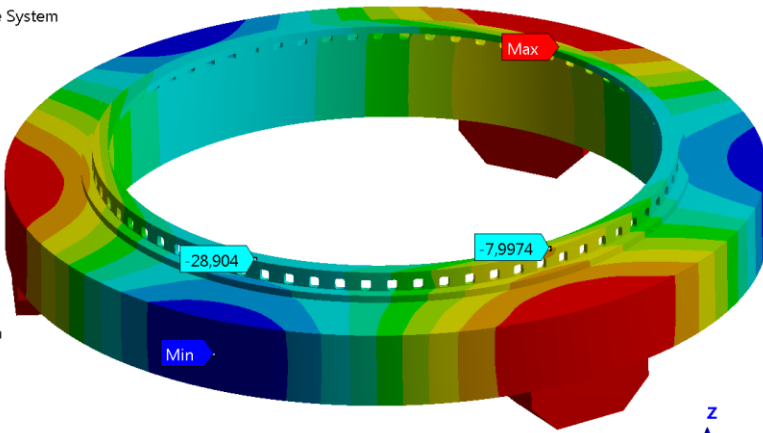
Mass 2636 Kg



Mass 1794 Kg

Directional Deformation
Type: Directional Deformation(Z Axis)
Unit: μm
Global Coordinate System
Time: 1
27.10.2016 09:38

1,2724 Max
-3,0811
-7,4347
-11,788
-16,142
-20,495
-24,849
-29,202
-33,556
-37,909 Min

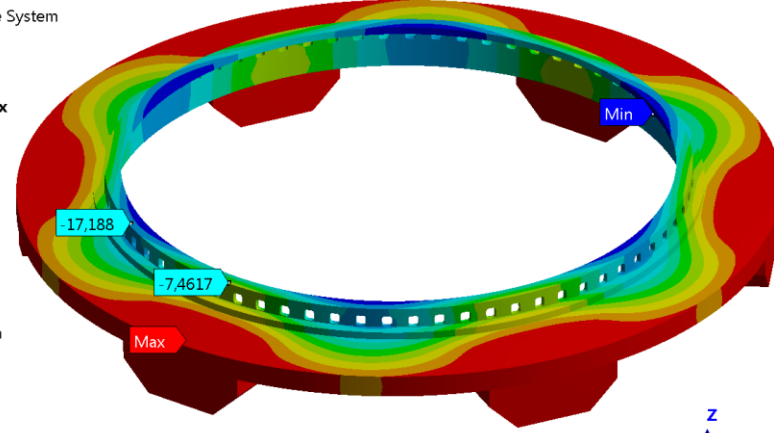


Deformation on the bearing 21 μm



Directional Deformation
Type: Directional Deformation(Z Axis)
Unit: μm
Global Coordinate System
Time: 1
27.10.2016 09:41

0,34456 Max
-2,0264
-4,3974
-6,7684
-9,1394
-11,51
-13,881
-16,252
-18,623
-20,994 Min

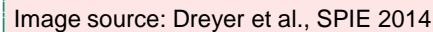


Deformation on the bearing 10 μm

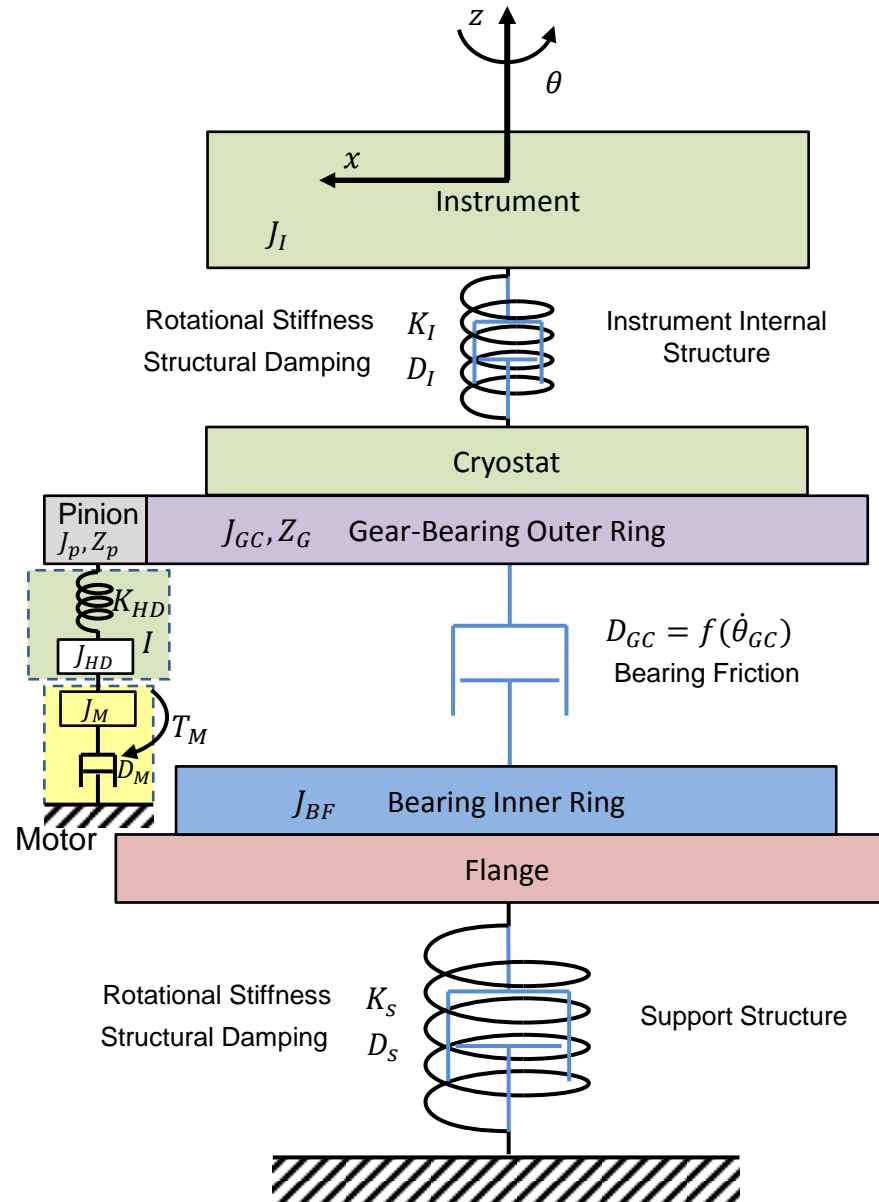
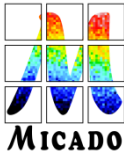


MICADO Derotator concept (support structure and motors not shown)

-
- ```
graph LR; TG[Trajectory Generator] --> M[Motor (Ideal)]; M --> C[Cryostat]; M --> G[Gear]; M --> B[Bearing]; M --> E[Encoder]; M --> S[Support structure]; BF[Bearing Friction] --> B;
```
- The diagram illustrates the mechanical components and signal flow of a cryostat system. A **Trajectory Generator** sends a signal to an **Ideal Motor**. The motor's output is distributed to a vertical stack of components: **Cryostat**, **Gear**, **Bearing**, **Encoder**, and **Support structure**. A **Bearing Friction** input is specifically directed to the **Bearing** component.



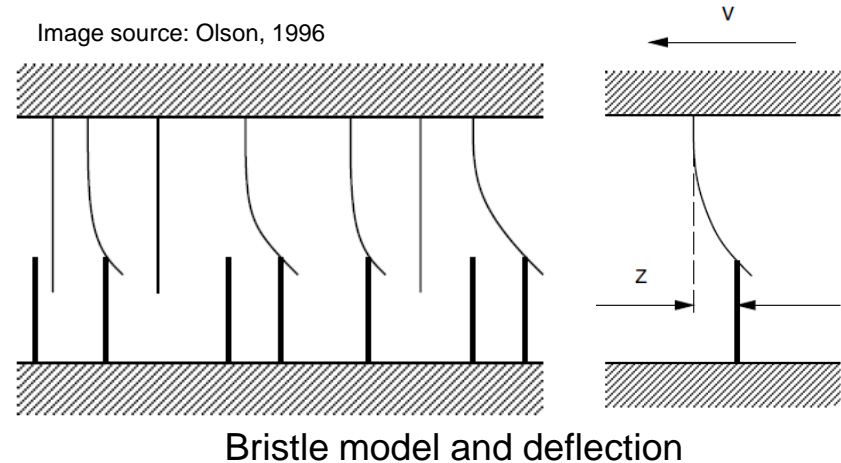
# MICADO Mechanical System





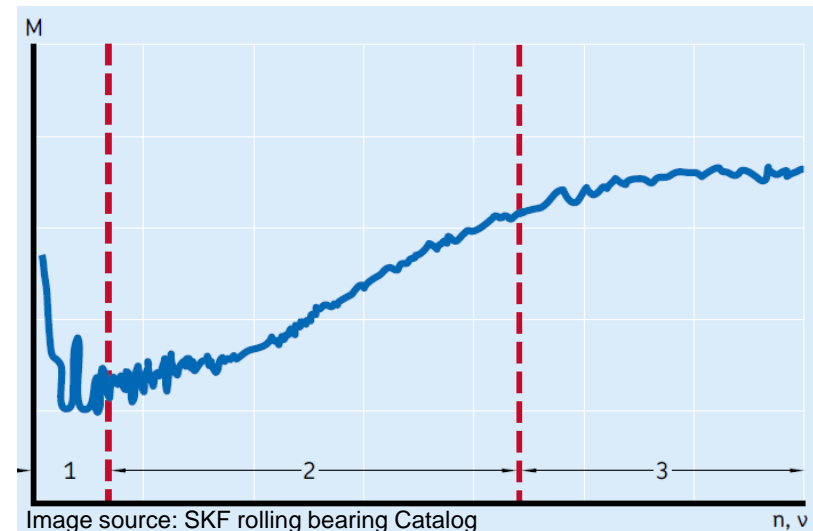
# Bearing Friction

- The LuGre Model (Olson, 1996)
  - The model is related to the bristle interpretation of friction
  - Friction is modelled as the average deflection force of the bristles (elastic springs)



- Parameters which have influence on the friction

- Rolling friction coefficient
- The rolling elements
- Cages or spacers
- Seals
- Load distribution
- The out-of-flatness of the support structure
- The grease filling
- The type of grease
- The lubrication of the lip seals
- The seal preload
- The variation in the bearing's clearance resulting from installation

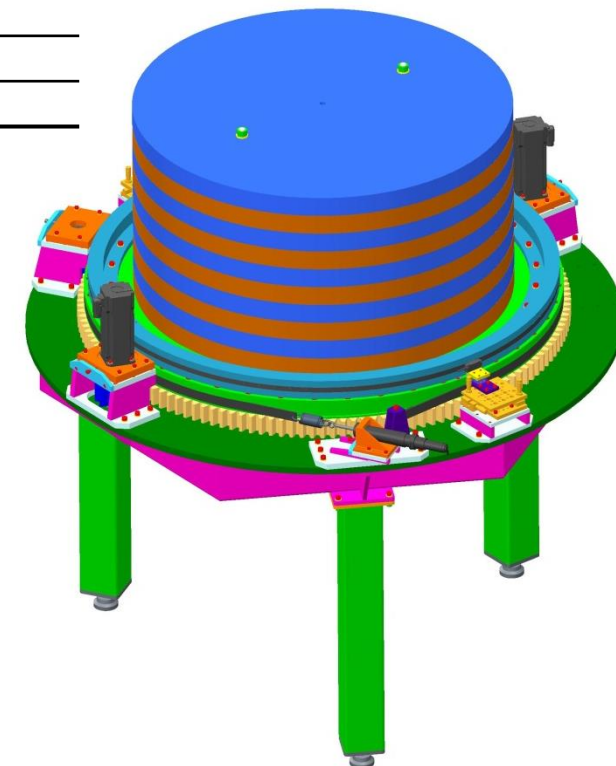


# Test Stand Kick-off Meeting (February 2016)

- Design of the experiment using an standard bearing

| Parameter                        | Test Stand Bearing     | Derotator Bearing     |
|----------------------------------|------------------------|-----------------------|
| Race way diameter                | 1094 mm                | 2290 mm               |
| Axial runout                     | $\leq 300 \mu\text{m}$ | $\leq 30 \mu\text{m}$ |
| Radial runout                    | $\leq 260 \mu\text{m}$ | $\leq 30 \mu\text{m}$ |
| Gear module                      | 8 mm                   | 6 mm                  |
| Number of teeth                  | 148                    | 403                   |
| Starting friction torque (0 rpm) | 1000 Nm                | 1800 Nm               |
| Running friction torque (1 rpm)  | 900 Nm                 | 1350 Nm               |

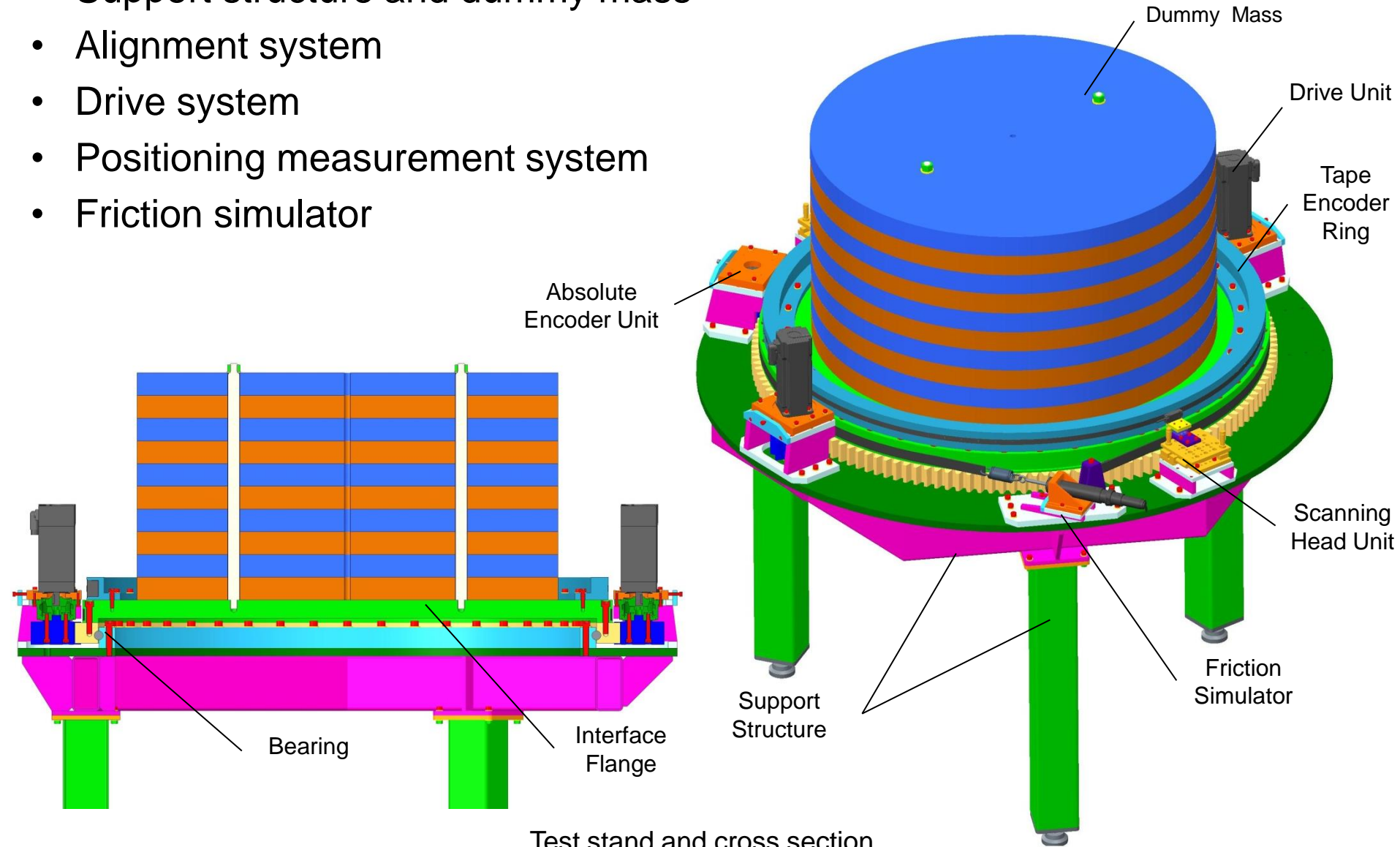
- Goals of the experiment
  - Learn about the implementation and performance of the tape encoder
  - Proof the alignment procedure between the interface flange and the bearing
  - Test backlash suppression system
  - Understand the effects of the friction over the positioning accuracy
  - Calibrate the parameters of the end-to-end model
  - Compare the results of the model with the performance of the real prototype
  - Validate the FEM of the bearing



Test stand

# Test Stand Components and subsystems

- Support structure and dummy mass
- Alignment system
- Drive system
- Positioning measurement system
- Friction simulator





# Drive system

- Servo motor Beckhoff AM8532D (rated torque: 2.2 Nm )
- Harmonic Drive (gear ratio: 160)
- Pinion with 12 teeth (gear ration: 12.33)

$$T_{TM} = K_S T_M = \mathbf{2.02\ Nm}$$

$$K_S = 1.2$$

$$T_M = \frac{T_{HD\ input}}{\eta_{HD}} = 1.68\ Nm$$

$$\eta_{HD} = 57\ \%$$

$$T_{HD\ output} = T_F + T_a = 0.96\ Nm$$

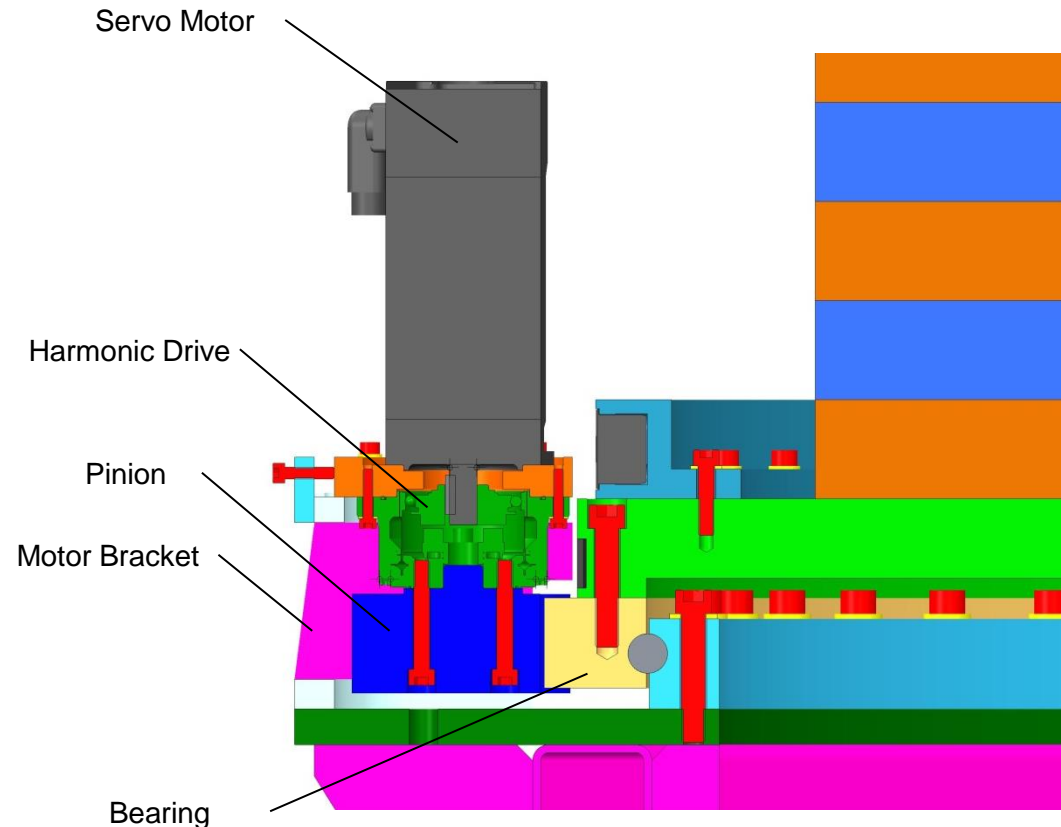
$$T_F = \frac{T_{FG}}{I_G I_{HD}} = \mathbf{0.917\ Nm}$$

$$T_{FG} = 1800\ Nm\ (\text{Rothe Erde})$$

$$I_G = \frac{Z_P}{Z_G} = 12.33$$

$$Z_P = 12, Z_G = 148, I_{HD} = 160$$

$$T_a = J_T \alpha = \mathbf{0.05\ Nm}$$



Drive system components cross section

# Positioning measurement system

- Integrated stator coupling absolute angle encoder (accuracy  $\pm 2.5''$ )
- Steel scale tape incremental angle encoder (accuracy  $\pm 1.9''$ ) plus Scanning head



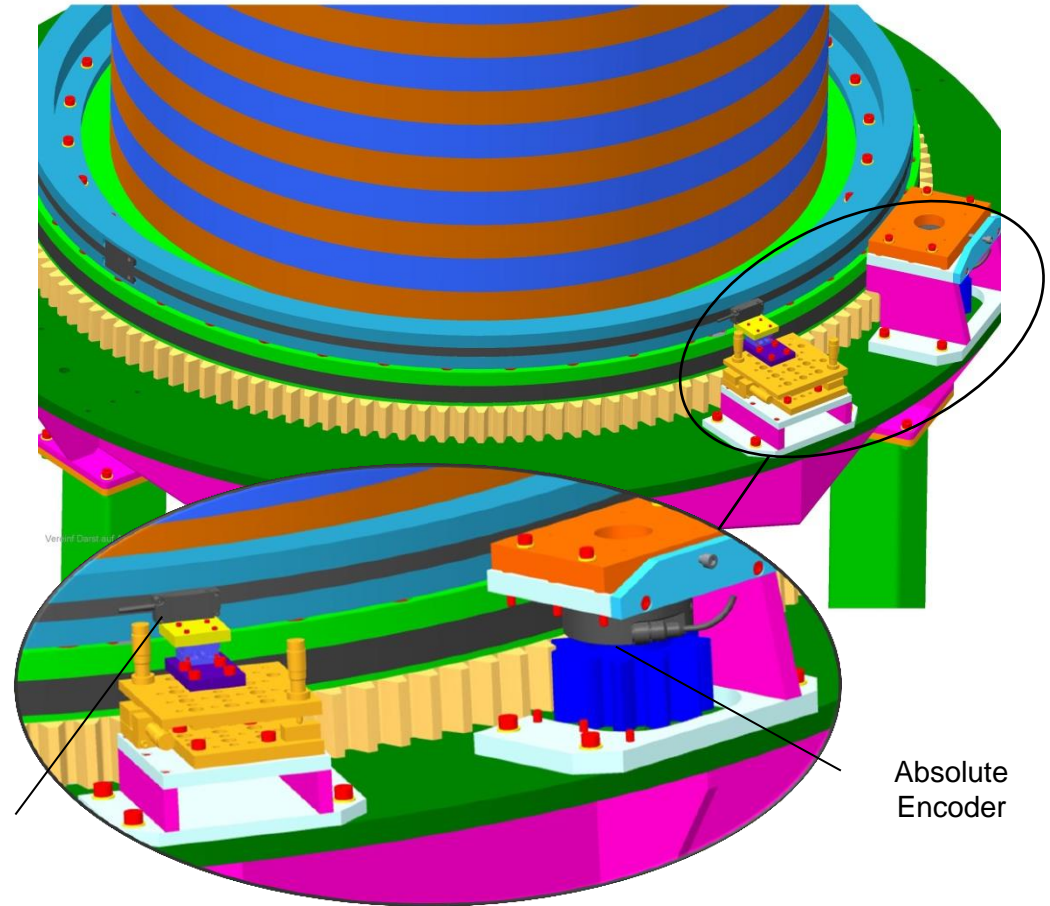
Heidenhain RCN 2000 Series



Heidenhain ERA 8000 Series

Image source: Heidenhain catalog

Tape Incremental Encoder  
and Scanning Head



Absolute  
Encoder

# Test Stand Integration Process



Test stand support structure and interface plate

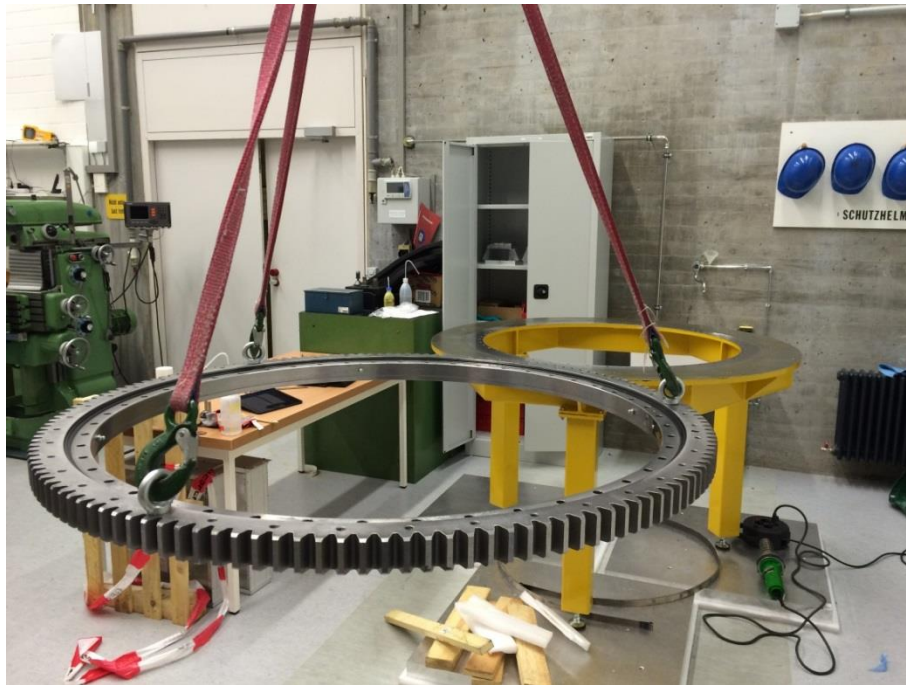


# Test Stand Integration Process



Encoder ring delivered by KINKELE, alignment pins and motor brackets by MPIA work shop

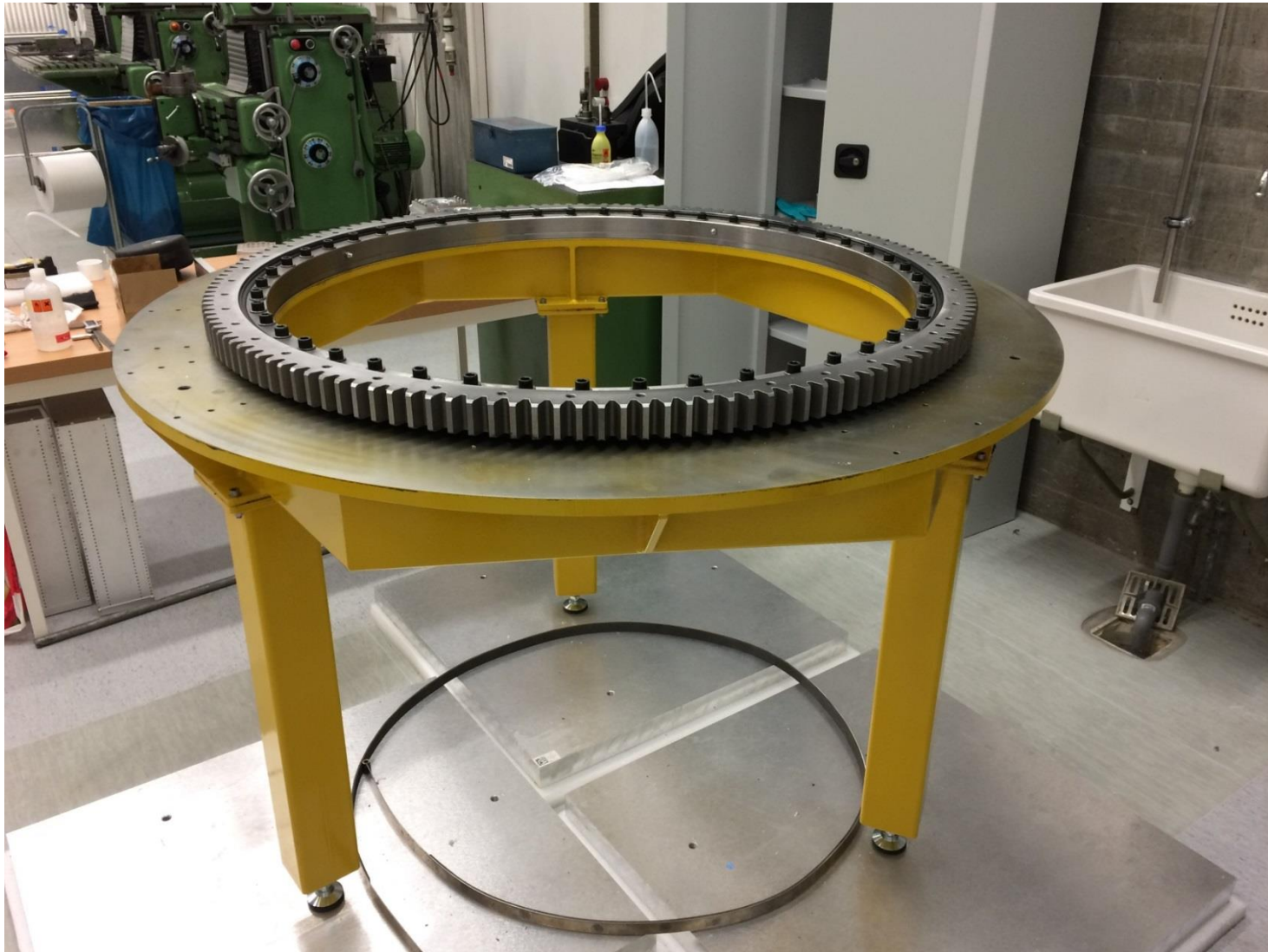
# Test Stand Integration Process



Standard Ø1.2 m bearing delivered by Rothe Erde



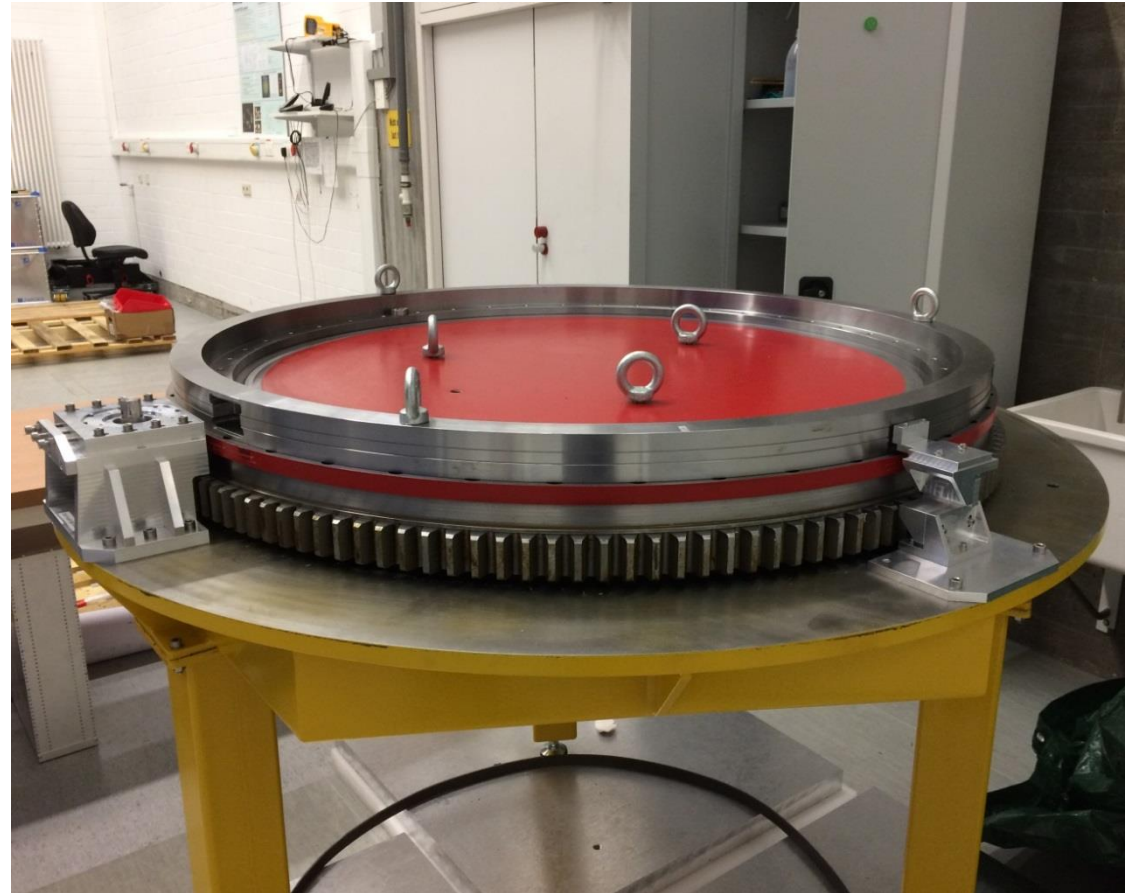
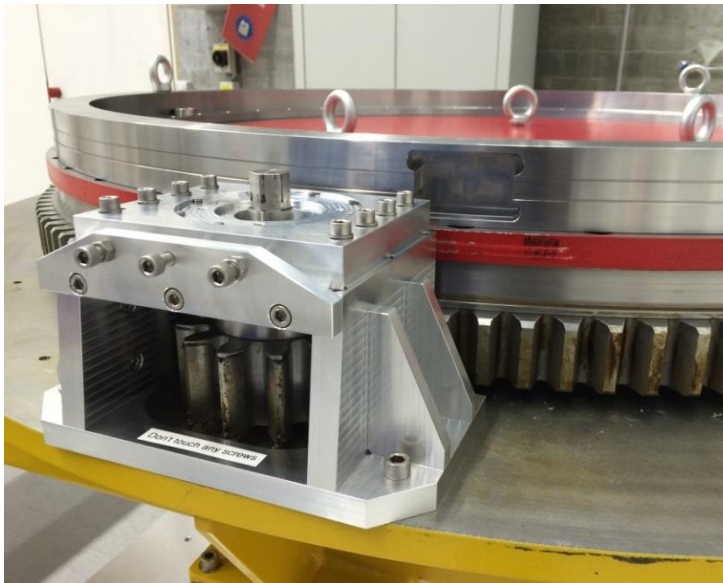
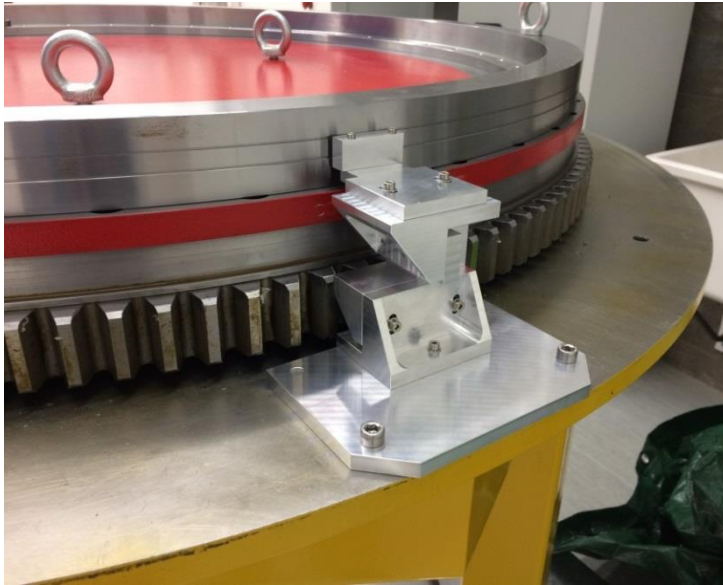
# Test Stand Integration Process



Bearing installed on the support structure

# Test Stand Integration Process

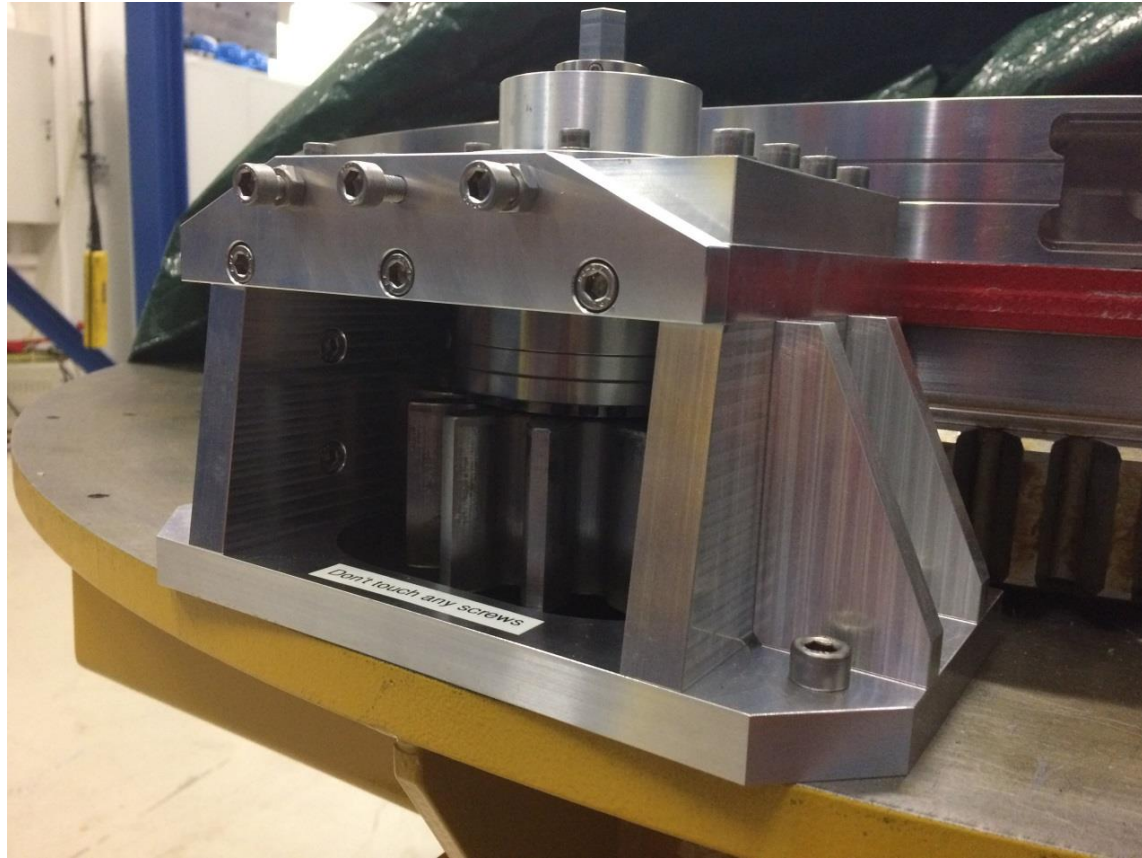
Status before the summer break...



Manual drive unit and encoder scanning head support

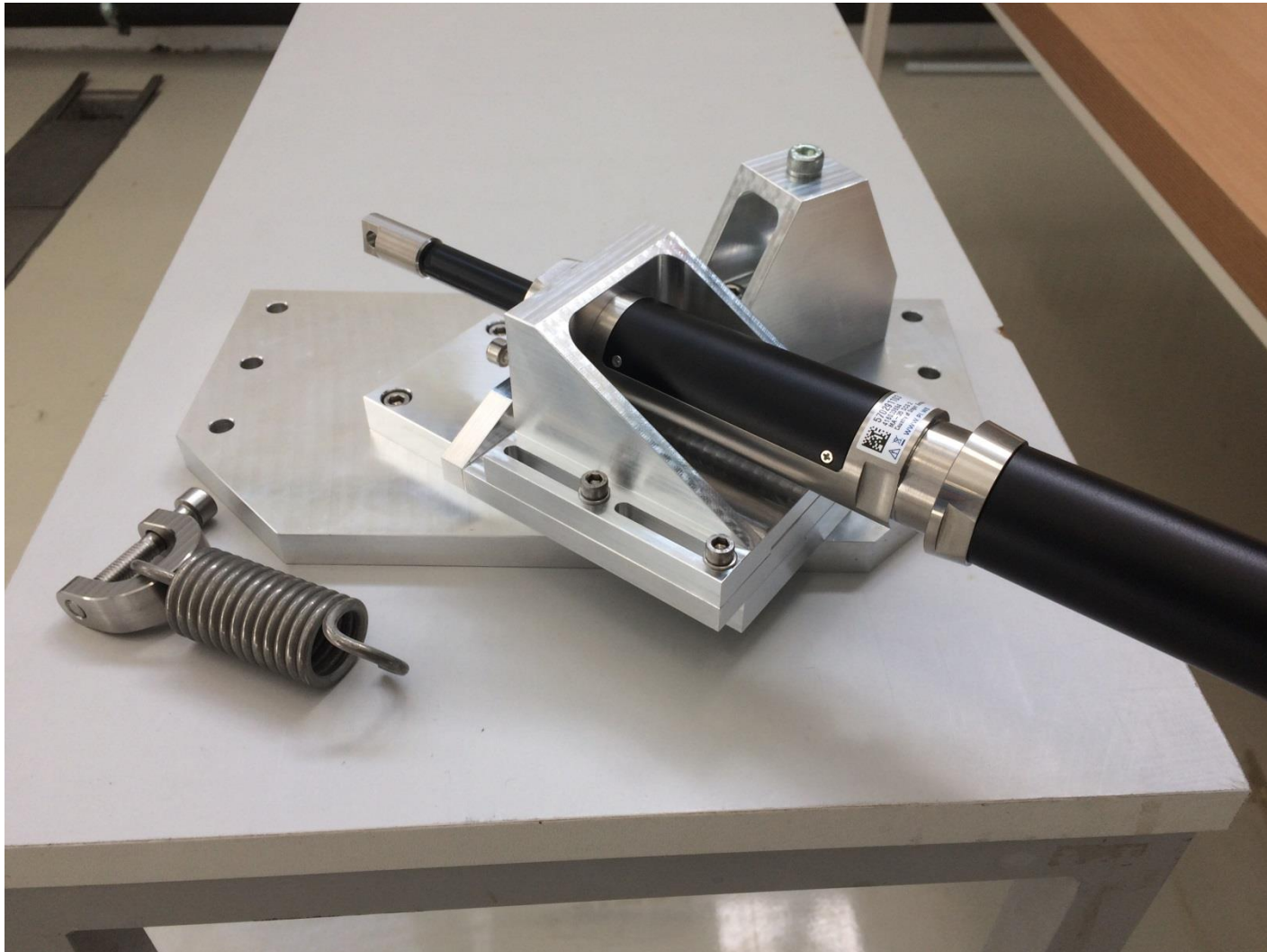


# Test Stand Integration Process



Drive unit test setup and manual drive unit with Harmonic Drive

# Test Stand Integration Process

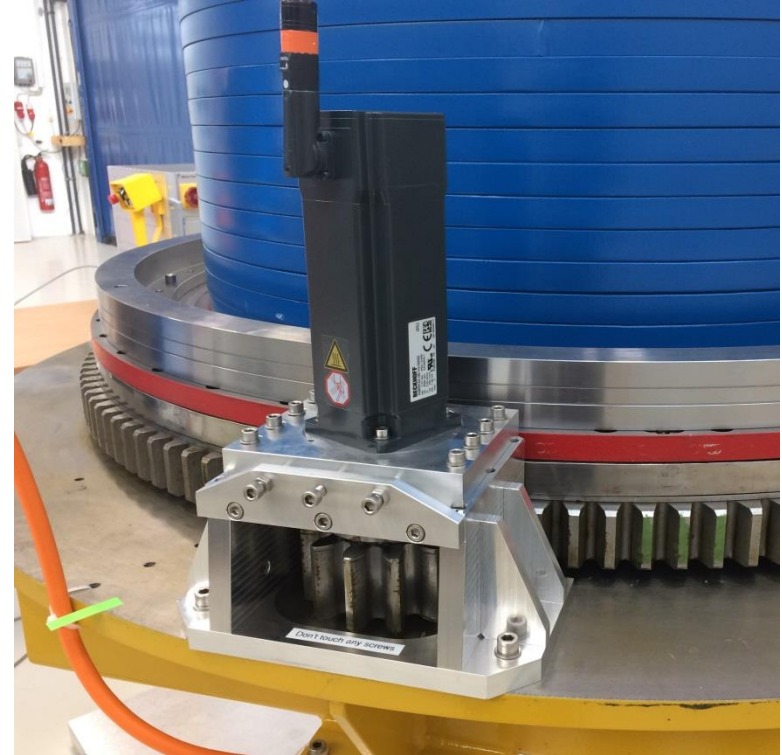


Friction simulator

# Test Stand Integration Process



Motor and electronic cabinet





# Test Stand Integration Process

- The real motor @ 1800 rpm / bearing @ 0.9 rpm / 3 tons

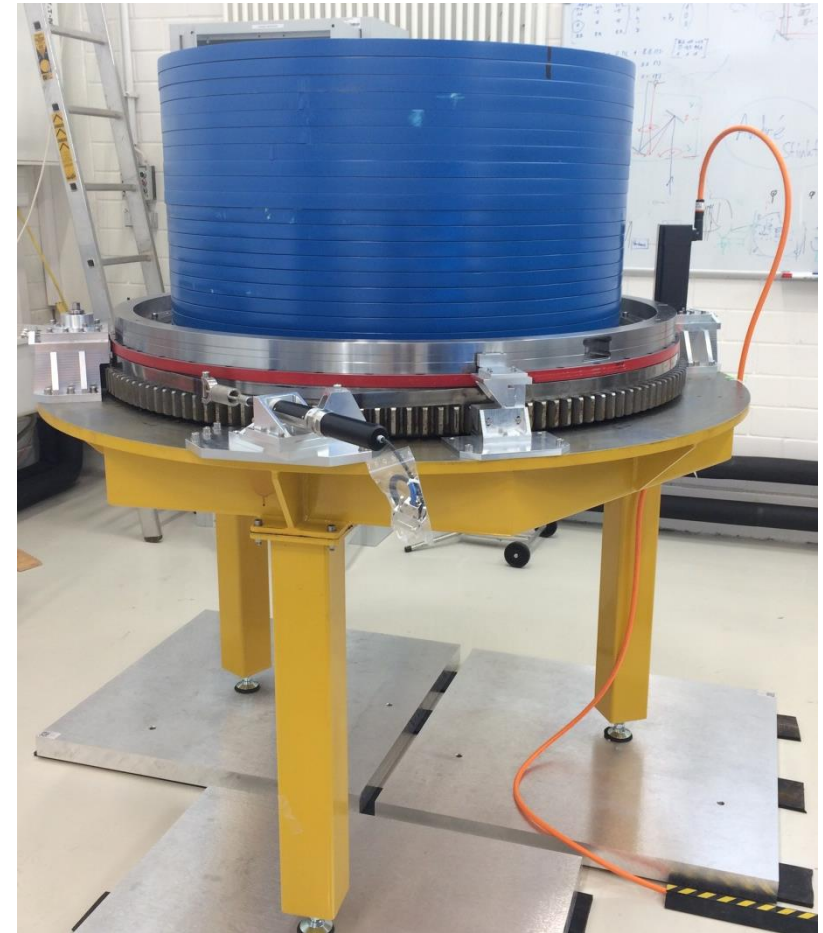
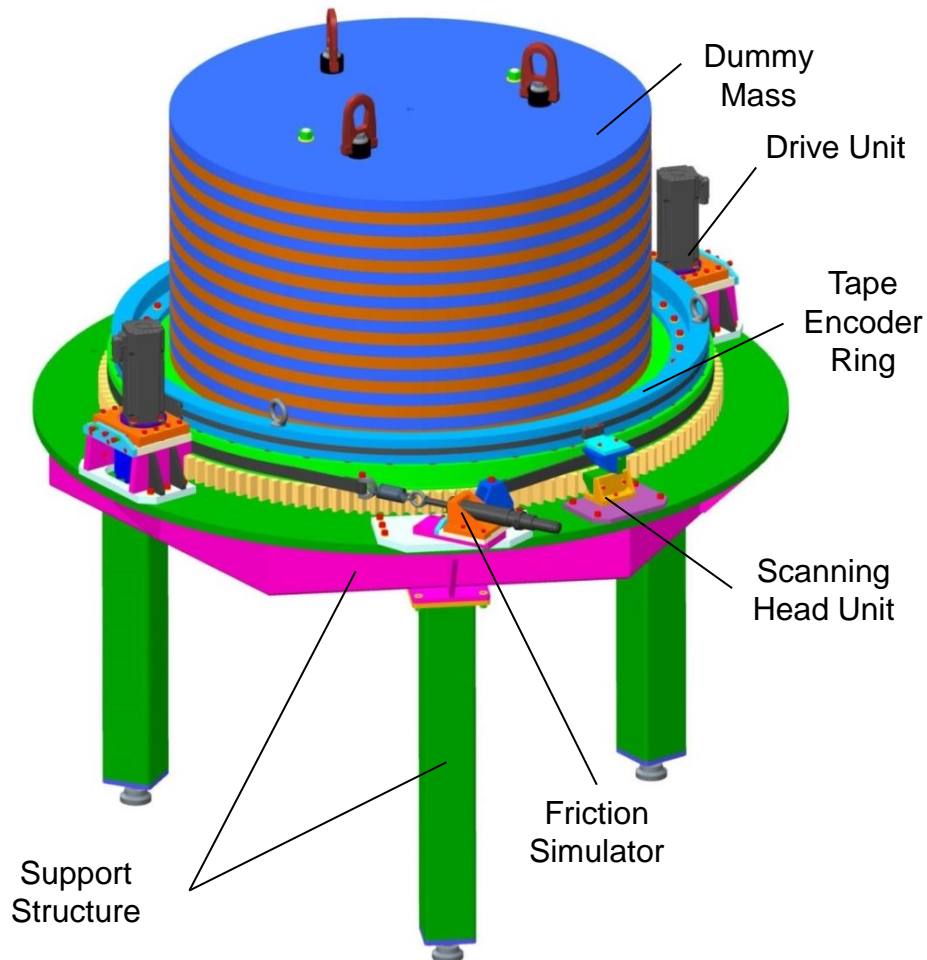


Motor and electronic cabinet



# Integration status and missing components

- Procurement and manufacturing “75%” (99%) completed
- Assembly and integration “75%” (90%) completed



Test stand CAD model (Kick of meeting February 2016) and real hardware

# Performance of the delivered bearing

| Parameter                               | Offered Bearing           | Delivered Bearing        |
|-----------------------------------------|---------------------------|--------------------------|
| Race way diameter                       | 1094 mm                   | 1094 mm                  |
| Axial runout                            | $\leq 300 \mu\text{m}$    | $\leq 50 \mu\text{m}$    |
| Radial runout                           | $\leq 260 \mu\text{m}$    | $\leq 60 \mu\text{m}$    |
| Wobble (calculated)                     | $\leq 113 \text{ arcsec}$ | $\leq 23 \text{ arcsec}$ |
| Starting friction torque (without mass) | 780 Nm                    | 300 Nm                   |
| Starting friction torque (with mass)    | 1000 Nm                   | 730 Nm                   |

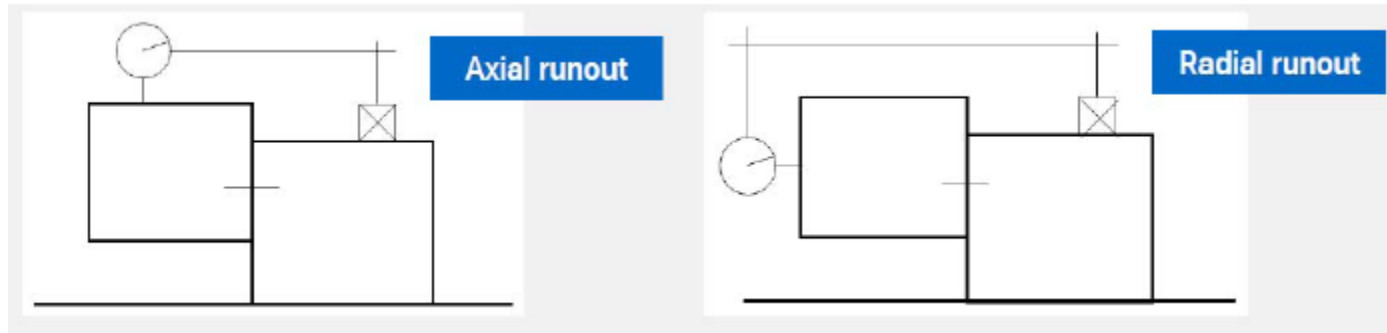
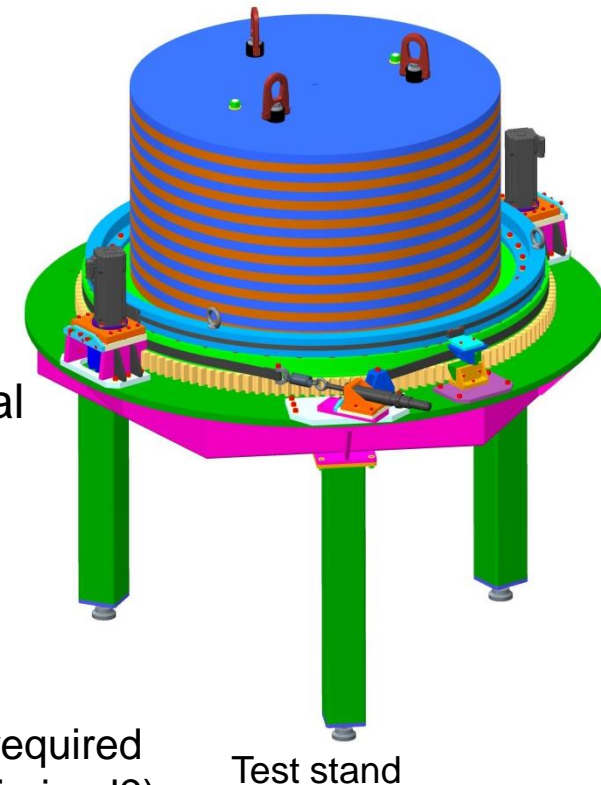


Image source: Rothe Erde

Measurement protocol performed by Rothe Erde

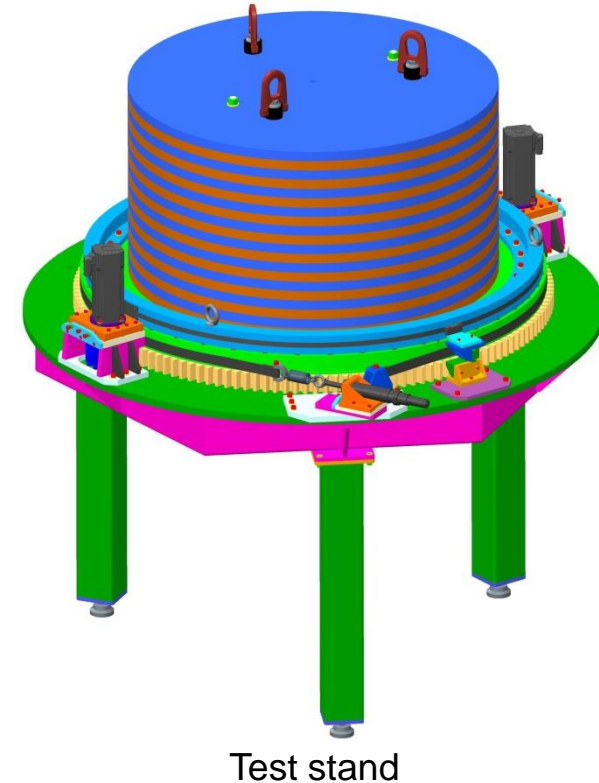
# Planning for the test campaign

- Test alignment procedure
    - Repeatability of the radial runout of the bearing
    - Alignment of the interface plate and the encoder ring to the bearing axis
    - Repeatability of the alignment system (with mass)
  - Measurement of the torque at the motor axis
    - Without mass
    - With mass (2990 Kg)
    - With mass and simulated **constant** friction of the real bearing (worst case)
  - Validate the FEM of the bearing
    - Measurement of the differential deformation on key points with load and without load
  - Test acceleration and speed
    - Time to rotate 360° with mass and friction
- Motor required (not optimized?)



# Planning for the test campaign

- Test the angular positioning accuracy (open and closed loop)
  - Without mass
  - With mass (2990 Kg)
  - With mass and simulated friction of the real bearing
- Test of the backlash suppression system
  - Define torque values between the pinions
  - Control system optimization
  - Measurement of the positioning accuracy over a trajectory with change of direction
- Calibrate parameters of the end-to-end model
  - Parameter identification of the drive unit
  - Parameter identification of the friction model
- Performance of the real prototype vs end-to-end model
  - Drive unit end-to-end simulation
  - Derotator test stand end-to-end simulation





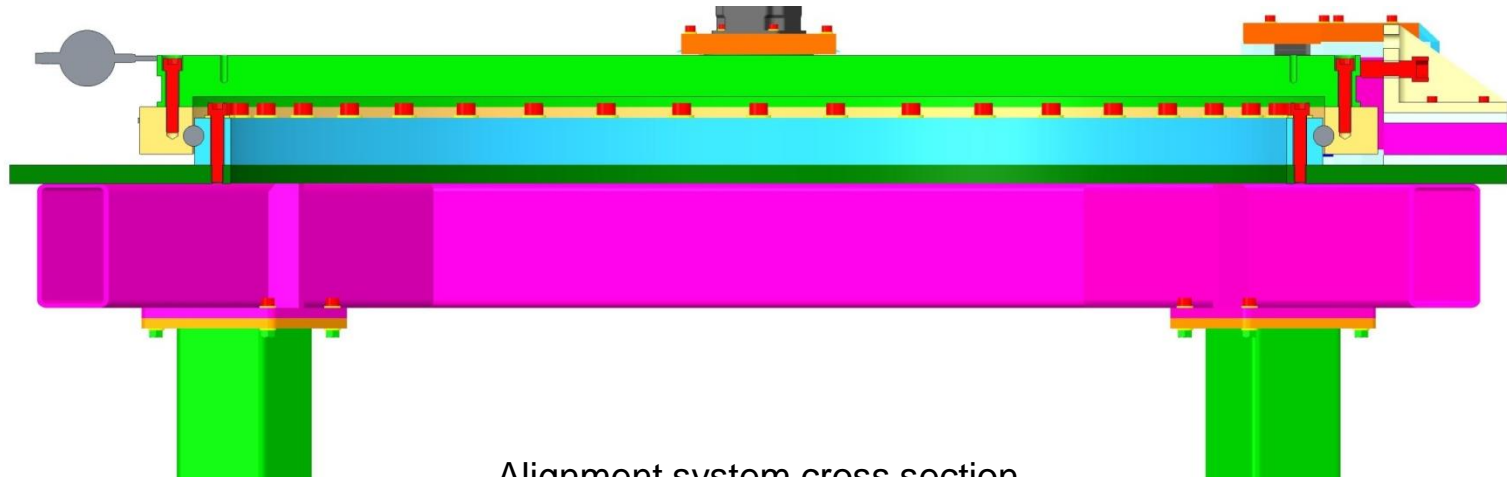
# Implementation schedule of the test campaign

- What have to be tested before the SRR?
- What can be done after the SRR?

| Items                                                        | October | November | December | January | February | March | April | May |
|--------------------------------------------------------------|---------|----------|----------|---------|----------|-------|-------|-----|
| Software development                                         | ?       |          |          |         |          |       |       |     |
| Test alignment procedure                                     |         |          |          |         |          |       |       |     |
| Measurement of the torque at the motor axis                  |         |          |          |         |          |       |       |     |
| Test acceleration and speed                                  |         |          |          |         |          |       |       |     |
| Validate the FEM of the bearing                              |         |          |          |         |          |       |       |     |
| Implementation of the encoder system                         |         |          |          |         |          |       |       |     |
| Test the angular positioning accuracy (open and closed loop) |         |          |          |         |          |       |       |     |
| Implementation of the friction system                        |         |          |          |         |          |       |       |     |
| Implementation with 2 motors                                 |         |          |          |         |          |       |       | →   |
| Test of the backlash suppression system                      |         |          |          |         |          |       |       | →   |
| Calibrate parameters of the end-to-end model                 |         |          |          |         |          |       |       | →   |

# Tests already performed

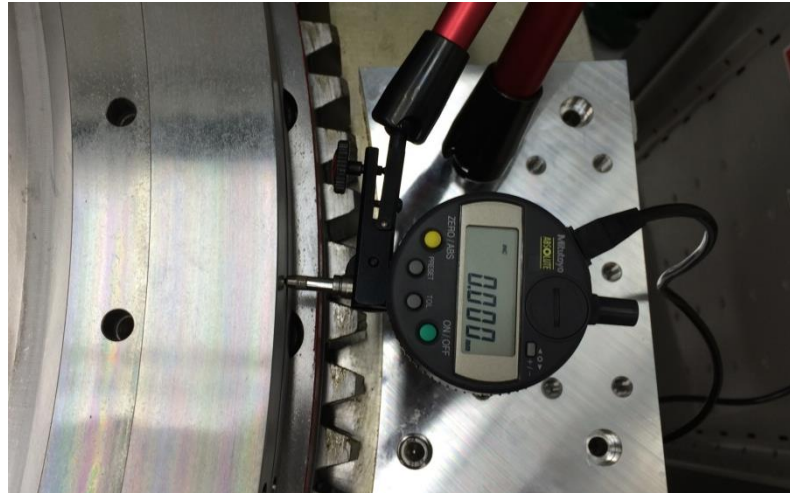
- Alignment procedure



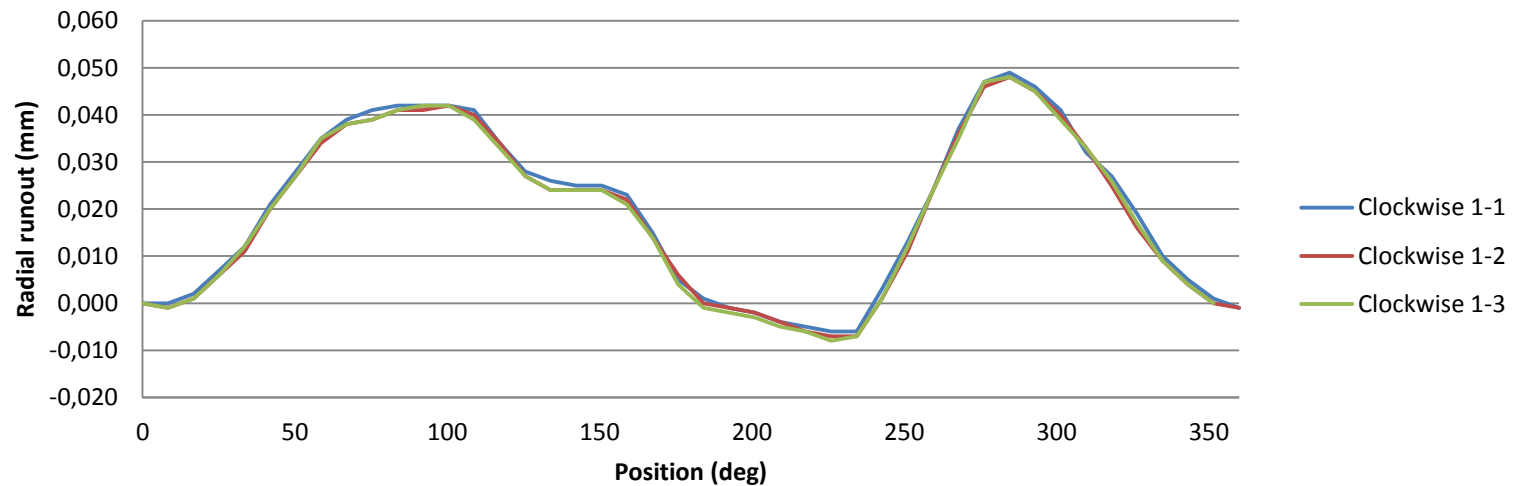
Alignment system cross section

# Tests already performed

- Alignment procedure of the encoder ring (radial runout < 0,05 mm)



Encoder ring



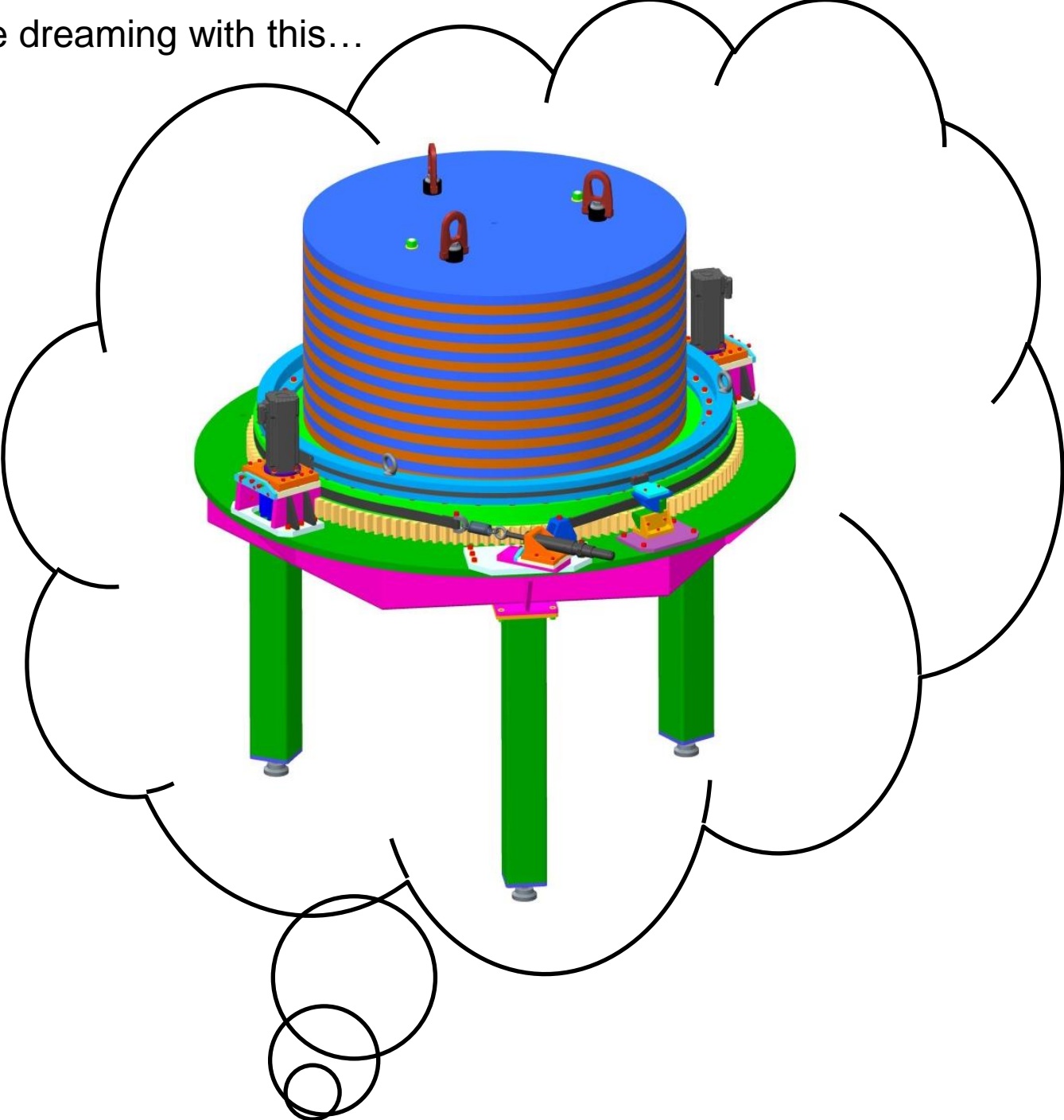


For inspiration...





Let's continue dreaming with this...



Let's continue dreaming with this...

